Transformable Cladding Systems: Research, Design and Fabrication

Clemens Lindner, Tao Sun Jonas Schikore, Prof. Dr. Pierluigi D'Acunto



Table of Contents

- Research Introduction Related work Categorisation Scientific Context
- Design Exploratory re
 - Exploratory research Targeted research: cable system Design selection
- Fabrication Profile Cable Parametrisation
- Insights
 - Potentials Weaknesses Application





Bachelorthesis Clemens Lindner¹, Tao Sun²

Supervisor: Jonas Schikore³, Prof. Dr. Pierluigi D'Acunto⁴

^{1.2,3,4}Technical University Munich (Professorship Structural Design)
^{1,2,3,4}{clemens.lindner | tao.sun | jonas.schikore | pierluigi.dacunto}@tum.de







Fig. 1: Historical cladding systems (chinese umbrella)

Research

Introduction

"Convertible roofs are designed so that their form can be changed as often as desired and in a relatively short time." (Blümel & Pankoke, 1972)

The ability to transform is also transferred to the corresponding cladding system. The traditional concept of architecture in the 20th century took durability and solidity as the most important characteristics of building as a given. This was gradually replaced by a concept that was characterised by functionality, practicality, utility and movement. (Blümel & Pankoke, 1972) These principles were pioneeringly explored by Frei Otto and his colleagues at the Institute for Lightweight Structures of the University of Stuttgart. Tents, awnings, street canopies, umbrellas, folding roofs and the Roman theatre velum have established themselves in various forms in our everyday lives worldwide over thousands of years (see Fig. 1). The fact that movement had previously played only a secondary role in architectural history has resulted in a lack of research in this area. This has led to the relevance of its research in recent years, as there are increasingly technical methods to parametrically simulate and statically calculate such technically highly complex constructions. This paper focuses on the research, design and digital fabrication of transformable cladding systems using the example of the Kinetic Umbrella project by Jonas Schikore from the Department of Technology/Structural Design at the Technical University of Munich.

Related work

An extensive research of typologies until the end of the 20th century is provided by the Institute for Lightweight Structures under the direction of Frei Otto in the book "Convertible Roofs IL 5" from 1972. Many different membrane constructions, their constructional details, and classification into different typologies are described based on the examples of built structures or concept designs (see Fig. 2). (Blümel & Pankoke, 1972)





Fig. 2: Umbrella-like structure

The doctoral thesis "Deployable Tensegrity Structures for Space Applications" shows different reflector antennas for space applications. The work also introduces several complex folding mechanisms (see Fig. 3) of transformable cladding systems for space applications. (Tibert, 2002)



Fig. 3: Deployment sequence of antenna

"Construction Manual for Polymers + Membranes" presents an overview of materials that can be used for transformable cladding systems, planning aids and built examples (see Fig. 4). It also lists convertible cladding systems with membrane systems. (Knippers, 2010)



Fig. 4: Trichterschirm

In his doctoral thesis, Motoi Masubuchi describes transformable foldable membrane roofs and their application and advantages. He explores different typologies, different materials, the historical background and carries out two case studies (see Fig. 5). (Masubuchi, 2013)



Fig. 5: Sequential view of membrane roof

In his work "Bending-Active Structures", Julian Lienhard describes the form-finding process for kinetic load-bearing systems with the help of elastic deformation (see Fig. 6). In particular, he examines the elasticity of different materials. (Lienhard, 2014)



Fig. 6: Wind tunnel tests

The dissertation by Zoran Novacki deals with a comprehensive overview and analysis of transformable linear load-bearing systems and the development of a new system (see Fig. 7) by combining existing typologies. (Novacki, 2014)



Fig. 7: Transformable load-bearing system

Andrej Mahovič examines rectable roof structures in stadiums and sporthalls and compares different systems and compares the opening and closing mechanism (see Fig. 8). (Mahovič, 2015)



Fig. 8: Tennis stadium Qizhong

Transformability has relevance in nature, as adaptation to the environment is essential for plants to survive. Numerous research projects explore the transformation and simultaneous adaptation of plants at different scales. Simon Schleicher shares his research report on bio-inspired compliant mechanisms for architectural design. He is inspired by flexible structures from nature and generates proposals for mechanisms with joint-free bending (see Fig. 9). (Schleicher, 2016)



Fig. 9: Kinetic model of the lily bud

"The geometry of unfolding tree leaves" mathematically describes the parallel folding method of leaves of hornbeam and beech from the blossom to the fully opened leaf. This complex folding method allows the very large leaf to be minimally folded (see Fig. 10). (Kobayashi et al., 1998)



Fig. 10: Hornbeam leaf



Fig. 13: Miura-ori pattern



"Structural, Deployable Folds - Design and Simulation of Biologically Inspired Folded Structures" focuses on the parametric calculation and translation of biologically inspired folded structures using earwigs, maple and hornbeam leaves as examples (see Fig. 12). (Baerlecken et al., 2014)



Fig. 12: Diagram of folding mechanism

In the paper "Self-Organized Origami", the folding mechanism of the hornbeam leaf is compared with the artificially generated Mira-ori folding pattern and its efficiency and mathematical derivation is described. (Mahadevan & Rica, 2005)

The hind wings of the bamboo weevil are similar to a convertible cover system are (see Fig. 11). Xin Li et al study this microstructure and simplify the principles of the folding mechanisms, thus providing a basis for reproducing them. (Li et al., 2019)





Sebastien J.P. Callens and Amir A. Zadpoor deal with the mathematical calculation and fabrication of curved geometries from flat sheets using origami and kirigami approaches. The resulting transformable systems all have the ability to shrink spatially. (Sebastien J.P. Callens & Amir A. Zadpoor, 2018)



Fig. 14: Concentric pleating origami

Guidelines for the parametric modelling and simulation of curved foldings are provided in the paper "Modeling Curved Folding with Freeform Deformations". The principles and geometric framework of curved folding are explained mathematically (see Fig 15). (Rabinovich et al., 2019)



Fig. 15: Comparison of the folding

Learning from mechanisms found in nature. Kathy Velikov et al. describes pneusystems as highly flexible structures that can be applied in architecture in a kinetic context. By inflating pneu cushions, structures can be designed which are not only extremely light and flexible, but also extremely controllable in their overall appearance (see Fig. 16). (Kathy et al., 2014)



Fig. 16: Nastic movement

Categorisation

The transformable structure and the associated transformable cladding system are proportionally dependent on each other. Therefore, we assume that they can be structured in the same way.

Based on the classification system (see Fig. 17) by Frei Otto of the Institute for Lightweight Structures in the book "Convertible Roofs IL 5" from 1972, our cladding system can also be categorised in this way. Ignoring the column construction system, convertible cladding systems can also be classified according to their type of movement: bunching, rolling, sliding, folding and rotating. These in turn can be classified according to their direction of movement: parallel, central, circular and peripheral.

In addition, it is important to note that these categorisations are not the only options. A combination of type of movements and type of directions can be made, which in turn creates new categories. New scientific findings can further add to the categorisation. For example, a pneu movement can be added as a new type of movement.



Fig. 17: Transformable structure classification

The aforementioned examples in the related work can be classified in the same way with the categorisation by the Institute for Lightweight Structures (see Fig. 17).

The built and concept designs by Blümel / Pankoke (see Fig. 2), the structure described in "Deployable Tensegrity Structures for Space Applications" (see Fig. 3), the "Trichterschirme" by Rasch+Bradatsch (see Fig. 4) as well as the roof of the Bull-fight ring in Jaén can be categorised as membranebased cladding systems with bunching and folding movements.

The examples of Julian Lienhard and Zoran Novacki showed in the figures 6 and 7, explored the possibilities of a new system achieved a covering system using a combination of folding and sliding movements.

In nature, folding surfaces mechanism can be found in both plants and animals. "The geometry of unfolding tree leaves" (see Fig.10) and the paper "Self-Organised Origami" (see Fig. 13) showcase the naturally

occurred rigid folding mechanism of the leaves of maple and hornbeam. Meanwhile, the non-folding joint-free flexible bending structure through the pneumatic cell movement found in plants (see Fig. 9) such as venus flytrap (see Fig. 16) suggest a new mechanism outside the categorisation of the Institute for Lightweight Structures. While in the realm of animals, the fan-shaped folded wings of earwigs and bamboo weevil (see Fig. 11 and 12) are investigated by Xin Li and Baerlecken et al.

Through advancements in the field of computational design, new possibilities for folding mechanisms have been invented and therefore expand the field of this research with complex curved folding mechanisms (see Fig. 14 and 15).



Fig. 18: Rendering of the Kinetic Umbrella

Scientific Context

The work, which has an interdisciplinary approach from architecture and structural engineering, focuses thematically on transformable cladding systems. Based on indepth research and analysis, the fabrication is exemplified using the Kinetic Umbrella project by Jonas Schikore.

With the Kinetic Umbrella, an innovative construction method is investigated. Straight lamellae are joined together to form a spatial grid structure by means of elastic deformation. Under consideration of geometric-mechanical rules, a grid structure is created which allows clearly defined deformations. When locked, the grid forms a highly efficient load-bearing structure. The aim is to generate a spatially changeable load-bearing structure by simple means and with little use of materials.



Students are closely involved in the development, production and construction of the Kinetic Umbrella project and learn about the relationships between spatial geometry,

Fig. 19: Sequence of the umbrella opening and closing

The Kinetic Umbrella changes shape from a 6.5 m high cylinder to an 8 m diameter umbrella (see Fig. 19). The supporting structure made of 32 GRP elements is activated by a cable system (actuation system). elasticity, tension and weight in a practical way.

The construction is part of a "researchby-design" process and will be put into operation on the event grounds of the Kreativquartier München after completion in summer 2021.

Design

Exploratory research

Based on the typologies of the previously identified structural systems and the geometric restrictions of the Kinetic Umbrella (see Fig. 8), first preliminary designs and concepts of transformable cladding systems are presented and compared in the categories:

- Weight (the cover system should be • light in order not to add unnecessary additional loads to the supporting structure, which could limit the transformability).
- Environmental (the covering system should provide protection against environmental influences such as wind, solar radiation and, if applicable, rain)
- Fabrication (the fabrication should be universally modular and digitally or easily fabricable, as a very large number is to be produced)
- Aesthetics (from an architectural point • of view, the covering system should complement the supporting structure and unite it aesthetically).



Fig. 20: Form change of rhombus

In this preliminary study, one unit of the Kinetic Umbrella is analysed individually (see Fig. 20). When closed, that module is a rhombus and is formed into a square by deforming the corner points. The resulting dependencies are complex and will be used in the following to create an efficient covering system.



Fig. 21: Form change of test model

In order to compare the different variations of this preliminary study from a qualitative point of view, a model was created which simulates the mechanical relationships of the Kinetic Umbrella in a simplified twodimensional space (see Fig. 21).



Fig. 22: Sketch: shingles, two points

Shingles - two points connected

The covering system with module-sized elements is adapted to the shape of the module when the umbrella is opened to the maximum. During the closing process, the shingles overlap more and more, but always remain connected to the structure at two points. (see Fig. 22)

Rainwater can drain off well as it is very overlapping in every opening position of the umbrella.





Fig. 24: Sketch: shingles, one point

Shingles - one point connected

The covering system with module-sized elements is also adapted to the shape of the module when the umbrella is opened to the maximum. During the closing process, the shingles overlap more and more, but always remain connected to the structure at one point. (see Fig. 24)

Rainwater can drain off well as it is very overlapping in every opening position of the umbrella.

The connection to the construction must be very durable as it must be able to withstand several forces impacting the connection point.





Fig. 26: Sketch: sliding, parallel

usage.

Sliding - parallel

The cover system with module-sized elements is adapted to the shape of the module when the canopy is opened to the maximum. During the closing process, the shingles overlap more and more, but always remain connected to the construction on two sides. (see Fig. 26)

Overlaps impale themselves to some extent with the construction and adjacent modules. 27). The variation is only sun protection. The cable construction is mechanically







Fig. 23: Photo: shingles, two points





Fig. 25: Photo: shingles, one point







Fig. 27: Photo: sliding, parallel





Fig. 28: Sketch: mechanical bunching

Bunching - automatic closing

The cover system with module-sized elements has a "curtain" that covers or opens the module proportionally to the opening and closing of the construction (see Fig.

interesting but complex and would therefore cause significant problems in everyday





Fig. 30: Sketch: folding, origami

Folding - Origami

The cover system consists of modular foldable elements. Each element has a relatively small thickness when folded and is positioned in the centre of each rhombus (see Fig. 29).

However, in the unfolded state, it only provides sun protection, not rain protection.

There is a higher vulnerability of the parts because they consist of a small-part folding mechanism.

Fig. 29: Photo: mechanical bunching



Fig. 31: Photo: folding, origami



Fig. 32: Sketch: folding, fan shaped

Folding - Fan shaped

The cover system consists of modular foldable elements. The folding mechanism consists of two overlapping compartments that close simultaneously with the construction (see Fig. 31).

In the unfolded state, it provides sun protection, but not reliable rain protection.

There is a higher vulnerability of the parts because they consist of a small-part folding mechanism.



Cable - Linear

The covering system with module-sized elements is covered with threads (see Fig. 33).

Therefore, no rain safety can be guaranteed.

It is possible to experiment with distances between the cables and with different cablecolours. In this way, complexity can be created.

Fig. 36: Sketch: cable, cross-module

Cable - cross-module

The covering system with cross-module elements is covered with threads (see Fig. 35).

Therefore, no rain safety can be guaranteed.

It is possible to experiment with distances between the cables and with different cablecolours. In this way, complexity can be created.





Fig. 38: Sketch: curved folding I.

Fig. 40: Sketch: curved folding II.

Curved folding II

Curved folding I

The covering system consists of modular foldable elements. Each element is relatively thin when folded and is located in the centre of each diamond (see Fig. 37).

In the unfolded state, however, it only provides sun protection, not rain protection.

There is a higher vulnerability of the parts because they consist of a small-part folding mechanism.

Curved folding means that the edges are not folded in a straight line but in a curved shape. This requires the use of machines or a very high amount of work.

mechanism. Only possible on every second module due to overlap.







Fig. 35: Photo: cable, linear





Fig. 37: Photo: cable, cross-module







Fig. 39: Photo: curved folding I.

Fig. 41: Photo: curved folding II.

10







The covering system consists of modular foldable elements. Each element is relatively thin when folded and is located in the centre of each diamond (see Fig. 39).

In the unfolded state, however, it only provides sun protection, not rain protection.

There is a higher vulnerability of the parts because they consist of a small-part folding





Fig. 42: Sketch: curved folding III.

Curved folding III

The covering system consists of modular foldable elements. Each element is relatively thin when folded and is located in the centre of each diamond (see Fig. 41).

In the unfolded state, however, it only provides sun protection, not rain protection.

There is a higher vulnerability of the parts because they consist of a small-part folding mechanism.



Fig. 43: Photo: curved folding III.

Concept	Weight	Environmental	Fabrication	Aesthetics	
Shingles two points connected	medium	sun + /rain + /wind 0	easy	clean	
Shingles two points connected	medium	sun + /rain + /wind -	easy	not matching structure	
Sliding parallel	heavy	sun + /rain + /wind -	difficult	not matching structure	
Bunching automatic closing	heavy (mechanism)	sun + /rain - /wind -	difficult	sophisticated	
Folding Origami	heavy	sun + /rain 0 /wind -	difficult	sophisticated	
Folding Fan shaped	medium	sun + /rain - /wind -	difficult	not matching structure	
Cable Linear	light	sun 0 /rain - /wind +	easy	clean/matching structure	
Cable cross-module	light	sun 0 /rain - /wind +	easy	clean/matching structure	
Curved folding	heavy	sun + /rain + /wind -	difficult	sophisticated	
Curved folding	ed folding heavy		difficult	sophisticated	
Curved folding	heavy	sun + /rain - /wind -	difficult	sophisticated	

Fig. 44: Overview of different cladding systems

Evaluation of the results

After the first preliminary study, all results are compared in an overview (see Fig. 44) on the basis of previously determined subjective and objective factors.

The shingle variants (with two and one connection point to the structure) (see Fig. 22, 24) are not considered as interesting, as they cannot withstand the wind forces on the Kinetic Umbrella due to their large-area covering.

The sliding solution (see Fig. 26) was not considered, as it was too complicated to build during the prototype test, as the sliding mechanism is very complex to construct and is too susceptible to long-term use

Likewise, the bunching mechanism (see Fig. 28) is too sensitive to environmental factors. The mechanism is very sophisticated and aesthetically very interesting. It considers the dependencies of the geometric relationships of the rhombus during deformation of the Kinetic Umbrella.

The folding mechanisms (origami and fanshaped) (see Fig. 30, 32) are too susceptible to wind forces due to their large-scale closure when the umbrella is open, but they are too time-consuming to fabricate. It is also a disadvantage that, despite their large-area covering, they do not offer any rain protection.

The curved folding variants (see Fig. 38,40,42) are also not interesting to develop further for the Kinetic Umbrella, as they cannot be manufactured in such a high quantity due to both their complex construction and high susceptibility to wind forces. In addition, a heavy material is needed for the folding mechanism to ensure that the geometry folds back again.

The cable system (see Fig. 34,36) is the most interesting to develop because it is simple to manufacture and also light. Moreover, from an aesthetic point of view, it

corresponds to and complements the Kinetic Umbrella. As this concept is simple at its core, it can be made more complicated in further steps, as there are many parameters that can be modified.

Some of the other concept ideas presented can also be developed further, but in our work we focus on cable systems exemplified on the kinetc umbrella project.

01. Orientation

.

.

- parallel to lamellas
- perpendicular to the lamellas





02. Layer for cable system integration

- bolts fixture
- upper lamella edge
- in lamella (outside)
- centre
- in lamella (inside) .
- lower lamella edge



03. Mounting method

profile

•

- drilling .
- punctual mounting
- cut-in



04. Cable Properties



- stiff
- foldable

.

.

flat





05. Parameterisation

- cable thickness
- cable colour
- cable distance





Targeted research: cable system

parameterisation.

the next step.

Cable systems on the Kinetic Umbrella have numerous parameters, most of which are dependent on each other or complement each other. Figure 45 shows an overview of all parameters: orientation to the lamellae of the Kinetic Umbrella, layer for the cable system integration, the mounting method, the cable properties and the

The design is based on a compilation of all parameters and a subjective consideration as well as consideration of the geometric constraints for installing the cover system on the Kinetic Umbrella. Taking all the above factors into account, an architectural concept is then developed and fabricated in

The orientation of the Kinetic Umbrella allows two directions: parallel to the outer lamella and perpendicular to the outer lamella (see Fig. 46). The outer lamellae were specifically considered as a reference, as the cabel system can follow or oppose them for an outside observer.



Fig. 46: Orientation comparison

The second parameter is the layer in which the cable system is integrated into the structure of the Kinetic Umbrella. For this purpose, a junction point is used at which the different layers can be identified exemplarily: bolts fixture, upper lamella edge, in

The third parameter is the mounting mehod, which is closely related to the previous parameter. Cables can be spanned or guided from lamella to lamella by numerous methods. The following have become established: profiles, drilling, punctual mounting and cut-in (see Fig. 48).





The preceding list of possible parame-

ters allows a subjective selection for the

implementation of the Kinetic Umbrella. In

the following, the individual parameters are presented. These were determined in an

iterative design process with consideration

The orientation of the cladding system will

therefore be parallel to the outer lamellae in order to make the construction more

The layer for the cable system integration

will be in the centre, as this hides the rear

readable from the outside.

of the geometric project-specific factors.

Design selection



Fig. 49: Pattern / colour study using water colour

Another important parameter is the properties of the cable. On the one hand, it can be distinguished by its properties: stretchable, stiff and foldable. On the other hand, it can have different geometric cross-sections. The most common are flat and round.

In the final step, the cable system can be parameterised. This is closely related to the other parameters. For example, the cable thickness, the cable colour and the cable distance can be used to create an interesting pattern. Conceptual watercolour

drawings were made to visualize this (see Fig.49).



Fig. 50: Pattern / colour study on the 1:3 model cut-out

In an experimental form-finding study, numerous possibilities were tested in a 1:3 segment of the Kinetic Umbrella. The figure on the left (see Fig. 50) shows the following configurations: elastic tensioned opening (1), cables fixed with single hooks (2), cables tensioned over profile (3), cable tensioned over L-profile (4), elastic tensioned textile (5), cables tensioned in two directions (6), coloured cables (7), drilled connection (8) and stretched rubbers (9).



A flat cable is selected in order to ensure a wide-area coverage with cable. This can provide more shade. In addition, fewer cables need to be installed to achieve the ficial. In addition, a slight stretching of the cable is required to compensate for certain inaccuracies.

The parameterisation is done by changing the density of the cables. This again reduces the cable length and has financial and aesthetic advantages at the same time. Moreover, parameterisation with colours makes the covering system more complex and corresponds to the phenomenology of the cable, as it is very easy to dye textiles.

Subsequently, all parameters can be summarised:

- parallel to outer lamellae
- centre layer cabel system integration
- discreet profile
- flat. strechable cable
- density and colour parameterisation

This example is only one possible variation of the Kinetic Umbrella's cover system, but it is used to illustrate the whole design process from concept to fabrication. It is developed in close collaboration with Jonas Schikore, Prof. Pierluigi D'Acunto (Technical University Munich) and Prof. Eike Schling (Hong Kong University).

Fig. 52: Gap issue

invalid length of profile

valid length of profile

A discreet profile is preferred so that the cover system is not perceived as a new structure. Drilling or other manipulation of the lamellae will damage them and hinder the opening and closing mechanism. The profile should also be easy to install.

same effect, which can be financially bene-



Fig. 51: Valid profile length



Geometric constraints

The defined parameters lead to geometric constraints, which are described and solved in the following.

During the prototyping process of the profiles, a geometric problem occured. If the bands are evenly distributed on the existing area along the lamella, the eccentricity of the node points causes the bands to be squeezed in the peripheral area (see Fig. 52).

Figure 51 shows the resulting distances from the lamella to the profile. It can be as much as a third of the total coverage (especially in the top modules) and is therefore problematic as it results in insufficient protection from the sun.

A possible solution to this problem is to move the position of the profile away from the eccentricity and towards the position of the node points. This has the consequence that the profiles have to be mounted with distance to the lamellae, but has the freedom to mount the cables freely on the entire profile.

Z



Fig. 53: Stripe-wise fixation

Another problem is that by opening the Kinetic Umbrella structure, the length of the cables differs. Since the profiles are intended to guide the cable, the cable is not precisely parallel to the lamellae, but instead follows a polyline with a seconddegree curvature and does not have a third-degree curvature like the lamellae of the structure.



Cable length (open) Cable length (closed) (min. 480.5 cm -(min. 482.3 cm max. 538.7 cm)



As an example, one module of the Kinetic Umbrella is analysed (see Fig. 53) and the length variation is compared in relation to the opening and closing of the structure.

The analysis shows that if the rope runs parallel to the outer lamellae, it must stretch by a maximum of 6 cm in the closed position of the Kinetic Umbrella (see Fig. 54).

max. 545.3 cm) max. 6.6 cm)

> This is not out of proportion, but cannot be ignored. A cable with a length change of at least 1cm per metre must be found to compensate for the calculated tolerance.

Cable length (open-closed)

(min. 1.8 cm -

This also applies to the cable direction perpendicular to the front lamellae (see Fig.55, 56).



Cable length (open) (min. 26.1 cm - max. 89.2 cm)

Cable length (closed) (min. 26.1 cm - max. 88.8 cm)

Cable length (open-closed) (min. 0.03 cm - max. 0.82 cm)

Fig. 56: Unit-wise length comparison

Fig. 57: Cull pattern diagram

metric constraints.

When creating a parameterisation with different densities, further problems occur

The width of the cable always remains the same and the cables must always be evenly distributed due to the geometry of the rhombus in the transformation process when opening and closing the Kinetic Umbrella and must not run diagonally, but always have a correlation point at the corresponding position on the profile. Due to this, when the modules become smaller, the cables overlap on the profile (see Fig. 57).

Figure 58 shows how a tolerance between the profile openings can be maintained by skipping every second cable. As a result, only a cull pattern of "0-1" ("delete every second cable") can be applied and cables cannot be selected randomly, as it is easier from a fabrication point of view to have cables start and end as few as possible.

Fig. 58: Tolerance issue

Ζ

59.

This means that in the lower modules there is a low density, as it goes up the cables become denser, and the cover system protects more from the sun. Since the sun shines in more from above, this makes sense. This effect is ideal, as it not only makes sense, but also makes the Kinetic Umbrella aesthetically appealing.

The resulting cables of different lengths, which always alternate on the profile, can then be coloured in different shades of grey and thus complete the desired design. The design is thus a combination of aesthetic subjective choices, geometric constraints and project-specific requirements (see Fig. 59).

Clemens Lindner | Tao Sun

on the profile, which lead to additional geo-



The final resulting pattern is shown in figure



Fig. 59: Cull pattern



Fig. 60: Isometric view of the resulting design

				13/50 = 4.85m 9/50 = 4.90m 13/50 = 4.90m 17/50 = 4.99m 21/50 = 5.04m 25/50 = 5.09m 29/50 = 5.13m 33/50 = 5.18m 37/50 = 5.23m 41/50 = 5.27m 45/50 = 5.37m	3 50 = 4.29m 7'50 = 4.34m 11'50 = 4.38m 15'50 = 4.47m 23'50 = 4.47m 23'50 = 4.52m 27'50 = 4.56m 31'50 = 4.65m 39'50 = 4.70m 43'50 = 4.79m	largest module is created, as can be seen in Figure 60. In Figure 61, an overview of the unrolled appearance of a strip of the Kinetic Umbrella is given. That will serve as a refe- rence for the planning of the fabrication.
				dark grey 2'50 = 2.53m 4'50 = 2.54m 6'50 = 2.56m 8'50 = 2.58m 10'50 = 2.58m 12'50 = 2.61m 14'50 = 2.62m 16'50 = 2.62m 16'50 = 2.62m 20'50 = 2.67m 20'50 = 2.67m 20'50 = 2.67m 20'50 = 2.67m 20'50 = 2.71m 26'50 = 2.71m 30'50 = 2.74m 30'50 = 2.77m 36'50 = 2.78m 34'50 = 2.78m 38'50 = 2.80m 40'50 = 2.81m 42'50 = 2.84m 46'50 = 2.87m 50'50 = 2.89m	odulo): 188 61 m	
				total length (mo total length: 30	odule): 188.61 m 17.76 m	

Fabrication

In the following, the previous theoretical solution is put into practice.

Profile

The profile, which contains all the geometric constraints, will now be designed in such a way that it is easy to manufacture, costeffective and easy to mount.

In a first step, different cut-outs are compared in a physical mock-up, which are lasered out of plastic (see Fig. 62).



Fig. 62: Laser-cut test profiles

An instability was detected when testing the lasered profiles. The expected flexibility of the profiles was too intense. In addition, fragile cut-outs can break off very easily. In a next attempt, profiles were milled out of aluminium (see Fig. 63). This requires digital fabrication, as the geometry must be highly precise (see Fig. 64). These profiles are also 1 mm thick, as this allows the desired flexibility. In addition, the cut-out with a rectangular cross-section is the most robust, although it requires the cable to be threaded.





Fig. 66: Profile test model



Fig. 63: Milled test profiles



Fig. 64: Milling process

Fig. 67: Mounting detail of profile



Fig. 65: Elevation of 1:1 model cut-out





The profile corresponds to the ideas and is tested on a 1:1 cut-out of the Kinetic Umbrella (see Fig. 65). With the help of distance pieces and M2 screws, the profiles are offset to the lamellae so that they are no longer eccentric (see Fig. 67).

Since the cover system experiences a certain tolerance due to both the mechanism of opening and closing the Kinetic Umbrella and due to construction inaccuracies, it is important that the profiles can be bent under load. This was tested in a small mock-up with the size of the smallest module, as this is the most difficult to deform (see Fig. 66).

Cable

As discovered in the design section, the cable has some aesthetic and geometric specifications.

Project-specific requirements are high UV protection and weather resistance, as the Kinetic Umbrella will be exhibited outdoors for an indefinite period of time. Material research has shown that polypropylene (PP) and polyethylene (PE) are very common in such an application. Natural materials are not as efficient in this regard.

Since a very large quantity of 3200 metres (includes a surcharge for cutting) is needed, the cable should be cost-effective.

In order to be able to save more material and at the same time provide more protection from the sun, a wider cable is preferred. It also requires a pre-calculated elasticity of at least 1cm per 100cm to allow elongation of the cable when opening and closing the Kinetic Umbrella and to prevent too much stress to the cable system.

First, commercially available cables were compared and benchmarked in Figure 69.

An evaluation of the results showed that none of the cables met all the necessary requirements. Most favoured was the "plus 400" baler twine from AGRI, but it was eliminated because it did not meet the desired aesthetics (see Fig. 68).

The "Umreifungsband" from Umreifung-24 is too rigid and cannot be steered as desired.



Fig. 68: Colour test

Image	Name	Price	Material	Diameter / Width	Property
Munumingenergingenergingenergingenergingenergingenergingenergingenergingenergingenergingenergingenergingenergin	Gummiseil STABILIT	1,85 €/m	rubber, PES	6 mm	highly elastic, UV+
unnaanna	PP-Seil STABILIT	0,80 €/m	PP, multifil	6 mm	non-elastic, UV++
	PP-Seil STABILIT	0,90 €/m	PP, multifil	15 mm	non-elastic, 45daN, UV+++
	Stahlraht-Seil, verzinkt STABILIT	0,80 €/m	zinc, steel	2 mm	non-elastic, 45daN, UV+++
	Starterleine STABILIT	0,60 €/m	PA	3 mm	non-elastic, 28daN, UV+++
an a	Reepschnur STABILIT	0,65 €/m	PP, multifil	3 mm	non-elastic, 19daN, UV++
	Stahlraht-Seil, PVC STABILIT	0,99 €/m	zinc, steel, PVC	2-3 mm	non-elastic, 45daN, UV+++
	Polyester 8 ROBLIN	0,59 €/m	PE	4 mm	non-elastic, 310daN, UV+
1910 International Constant	Orion 500 ROBLIN	1,39 €/m	PE	6 mm	non-elastic, 800daN, UV+
	plus 400 AGRI	0.01 €/m	PP	4 mm	non-elastic, 400daN,UV+
	Umreifungsband Umreifung-24	0.03 €/m	PE	7 mm	non-elastic, 350daN, UV+

Fig. 69: Cable overview



Fig. 70: Cable close-up view



Fig. 71: Elasticity test



Fig. 72: Form change of 1:1 model cut-out



In close cooperation with manufacturers from the textile industry, the next step is to customise a cable to meet all requirements. The Bavarian company Gepotex has offered to participate in the development of the cable. This resulted in a custom-made woven cable with the desired width of 7mm and UV and weather resistance (see Fig. 70).



The cable is woven from the material Diolen. It is characterised by its high tensile strength and its resistance to oxygen, light and high temperatures. It was woven in a special process so that it has the required elasticity. In an experiment, a 50 cm long piece could be stretched 59 cm with a force of 11.3N (see Fig. 71). When released, the cabel returns to its original state.

Afterwards the cable was tested on the 1:1 model in combination with the previously milled aluminium profiles (see Fig. 72). A metal clamper was used to fix the cables. The advantage of this is that it can be installed quickly and is stable at the same time.

Parametrisation

The final step of the fabrication is colour parameterisation. Each cable was dyed using the previously created pattern (see Fig. 61).

Half of the cables are coloured with dark grey, a quarter with light grey and the rest remains white. The individual cables can be cut to the correct length in advance and then bathed in dye. The colour must also guarantee weather and sun protection.

A colour prototype study is made on the same 1:1 module as in figure 72 to test the overall appearance (see Fig. 73).

The play of colours during the day creates a homogeneous colour gradient across the structure of the Kinetic Umbrella, thanks to the parameterisation. It is not just this that makes the project aesthetically outstanding, but also the fact that in the dark, the Kinetic Umbrella stands out by its varied use of light. While the white cables reflect more light, the darker ones reflect less. In this way, the homogeneous, parameterised colour gradient can also be perceived in the dark. An art installation by Jeongmoon Choi can serve as a reference for this (see Fig. 74).

Insights

Potentials

The resulting cladding system for transformable structures, using the example of the Kinetic Umbrella, can be universally seen as a cladding system for transformable structures, as it can be applied in a variety of configurations.

Due to its linearity, the flexible cable system is particularly suitable in combinations with grid structures, as they can emphasise their structure in this way. In the case of the Kinetic Umbrella, it also corresponds to the design language of the actuation system.

The simplicity of the manufacturing process and the easy installation in particular should give architects and clients confidence for transformable structures. The transformable cladding system turns the Kinetic Umbrella into an architectural structure that offers solar protection and invites visitors to linger beneath it.

Fig. 73: Colourisation on the 1:1 model cut-out



Fig. 74: LINESCAPE by Jeongmoon Choi

Application

One weakness of the transformable cladding system is that it only protects against the sun and not against rain. However, this was explicitly taken into account.

Weaknesses

It should also be mentioned that transformable structures result in numerous geometric constraints due to their complex geometry. However, this is also an advantage for the planner, as they can utilise them to their advantage in the planning process.

Furthermore, it must be mentioned that due to the small-scale nature of the designed concept, vandalism is very likely to occur.

In conclusion, however, it can be said that the advantages clearly outweigh the disadvantages. Since the construction of the Kinetic Umbrella is still in the planning stage and has not yet begun when this paper is published, the application is shown on a 1:3 model.

However, all individual steps have been tested on the 1:1 module and the construction can begin.

As can be seen in figure 75, 76, 77 and 78, the cladding system complements the Kinetic Umbrella very well and completes its overall appearance.



Fig. 75: Top view 1:3 model, open



Fig. 76: Front view 1:3 model, open



Fig. 77: Top view 1:3 model, closed



Fig. 78: Front view 1:3 model, closed

Bibliography

- Baerlecken, Daniel; Gentry, Russell; Swarts, Matthew in: SAGE Publications: Structural, Deployable Folds - Design and Simulation of Biological Inspired Folded Structures, London, 2014, S. 243-262, (ISSN 1478-0771)
- Blümel, Dieter: Pankoke, Uta in: Krämer: Convertible roofs. Stuttgart 1972. (OCLC 246762694)
- Kathy, Velikov; Thün, Geoffrey; O'Malley, Mary in: ACADIA 2014: Design Agency: Pneusystems. Cellular Pneumatic Envelope Assemblies, Los Angeles 2014, S. 435-444, (ISBN 9781926724485)
- Knippers, Jan in: Inst. für Internat. Architektur-Dokumentation: Atlas Kunststoffe + Membranen, Werkstoffe und Halbzeuge Formfindung und Konstruktion, München, 2010, (ISBN 9783920034416)
- Kobayashi, H.; Kresling, B in: The Royal Society: The geometry of unfolding tree leaves, London 1998, S. 147 -154, (ISSN 0962-8452)
- Li, Xin; Guo, Ce; Li, Longhai in: Taylor & Francis: Functional morphology and structural characteristics of the hind wings of the bamboo weevil Cvrtotrachelus buqueti (Coleoptera, Curculionidae), 2019, S. 143-153, (ISSN 1976-8354)
- Lienhard, Julian in: ITKE: Bending-active structures. Form-finding strategies using elastic deformation in static and kinetic systems and the structural potentials therein. Stuttgart 2014. S. 36-210, (ISBN 978-3-922302-36-0)
- Mahadevan, L. in: Science: Self-organized origami, New York 2005, S. 1740. (ISSN 0036-8075)
- Mahovič, Andrej in: University of Ljubljana, Faculty of Architecture and University of Liubliana. Faculty of Civil and Geodetic Engineering: Typology of Retractable Roof Structures in Stadiums and Sports Halls, Ljubljana 2014, S. 90-99, (ISSN 2350-3637)
- Masubuchi, Motoi in: Shaker: Conceptual and structural design of adaptive membrane structures with spoked wheel principle – folding to the perimeter, Berlin 2013, (ISBN 978-3844023046)

- Novacki, Zoran in: Lehrstuhl für Tragwerksplanung Technische Universität München Fachbereich Architektur: Wandelbare lineare Tragsysteme. Analyse und Neuentwicklung, München 2014, (ISBN 978-3938660287)
- Rabinovich, Michael; Hoffmann, Tim; Sorkine-Hornung, Olga in: ACM: Modeling curved folding with freeform deformations. New York 2019. (ISSN 0730-0301)
- Schleicher, Simon in: Universität Stuttgat Inst f Konstruktionstechnik u Technisches Design: Bio-inspired compliant mechanisms for architectural design. Dissertation, Stuttgart 2015, (ISBN 978-3922302407)
- Sebastien J.P. Callens; Amir A. Zadpoor in: Materials Today: From flat sheets to curved geometries: Origami and kirigami approaches, Delft 2018, S. 241-264, (ISSN 1369-7021)
- Tibert, Gunnar in: Royal Institute of Technology Department of Mechanics: Deployable Tensegrity Structures for Space Applications, Stockholm 2002, (ISSN 0348-467X)

List of Figures

- 0 Sun, Tao; Lindner, Clemens: Title image
- 1 Blümel, Dieter; Pankoke, Uta: Historical cladding systems, in: Krämer: Convertible roofs, Stuttgart 1972, (OCLC 246762694)
- 2 Blümel, Dieter; Pankoke, Uta: Built and conceptual umbrella-like structure, in: Krämer: Convertible roofs, Stuttgart 1972, (OCLC 246762694)
- 3 Tibert, Gunnar: Deployment sequence of the hoop/column antenna, in: Royal Institute of Technology Department of Mechanics: Deployable Tensegrity Structures for Space Applications. Stockholm 2002, S.21, (ISSN 0348-467X)
- 4 Knippers, Jan: Trichterschirm 10 ≈ 10 m. Stuttgart (D) 1990, Rasch + Bradatsch, in: Inst. für Internat. Architektur-Dokumentation: Atlas Kunststoffe + Membranen. Werkstoffe und Halbzeuge Formfindung und Konstruktion, München, 2010, S. 149, (ISBN 9783920034416)

- 5 Masubuchi, Motoi: Sequential view of retractable membrane roof from closed state to opened state (courtesy of Felix Escrig), in: Shaker: Conceptual and structural design of adaptive membrane structures with spoked wheel principle – folding to the perimeter, Berlin 2013, S. 22, (ISBN 978-3844023046)
- 6 Lienhard, Julian: Wind tunnel tests of twisted and planar membrane strips (Wacker Ingenieure - Wind Engineering), in: ITKE: Bending-active structures. Form-finding strategies using elastic deformation in static and kinetic systems and the structural potentials therein, Stuttgart 2014, S. 89, (ISBN 978-3-922302-36-0)
- 7 Novacki, Zoran (2014): transformable load-bearing system, in: Lehrstuhl für Tragwerksplanung Technische Universität München Fachbereich Architektur: Wandelbare lineare Tragsysteme. Analyse und Neuentwicklung, München 2014, S. 140, (ISBN 978-3938660287)
- 8 Mahovič, Andrej: Tennis stadium Qizhong Forest Sports City Arena, Mahovič, Andrej in: University of Ljubljana, Faculty of Architecture and University of Ljubljana, Faculty of Civil and Geodetic Engineering: Typology of Retractable Roof Structures in Stadiums and Sports Halls, Ljubljana 2014, S. 93, (ISSN 2350-3637)
- 9 Schleicher, Simon: Kinetic model of the lily bud, in: Universität Stuttgat Inst. f. Konstruktionstechnik u. Technisches Design: Bio-inspired compliant mechanisms for architectural design. Dissertation. Stuttgart 2015, (ISBN 978-3922302407)
- 10 Kobayashi, H.; Kresling, B.; Vincent, J. F. V.: Hornbeam leaf showing relatively regular corrugation, in: The Royal Society: The geometry of unfolding tree leaves, London 1998, S. 1581, (ISSN 0962-8452)
- 11 Li, Xin; Guo, Ce; Li, Longhai: The video sequence of the hind wings of C. buqueti unfolding, in: Taylor & Francis: Functional morphology and structural characteristics of the hind wings of the bamboo weevil Cyrtotrachelus buqueti (Coleoptera, Curculionidae), 2019, S. 148, (ISSN 1976-8354)
- 12 Baerlecken, Daniel; Gentry, Russell; Swarts, Matthew: Diagram of folding mechanism, earwigs, in: SAGE Publications: Structural, Deployable Folds

- Design and Simulation of Biological Inspired Folded Structures, London, 2014, S. 264, (ISSN 1478-0771)

- 13 Mahadevan, L.; Rica, S.: Plan view of a paper Miura-ori pattern, Hornbeam leaves, Zigzag Miura-ori, Simulations of Eq. 1, n: Science: Self-organized origami, New York 2005, S. 1740, (ISSN 0036-8075)
- 14 Sebastien J.P. Callens; Amir A. Zadpoor: Concentric pleating origami, in: Materials Today: From flat sheets to curved geometries: Origami and kirigami approaches, Delft 2018, S. 254, (ISSN 1369-7021)
- 15 Rabinovich, Michael; Hoffmann, Tim; Sorkine-Hornung, Olga: Comparison of the same deformation objective with and without our folding algorithm, in: ACM: Modeling curved folding with freeform deformations, New York 2019, S. 3, (ISSN 0730-0301)
- 16 Kathy, Velikov; Thün, Geoffrey; O'Malley, Mary: Nastic movement, in: ACADIA 2014: Design Agency: Pneusystems. Cellular Pneumatic Envelope Assemblies, Los Angeles 2014, S. 437, (ISBN 9781926724485)
- 17 Blümel, Dieter; Pankoke, Uta: Transformable structure classification, in: Krämer: Convertible roofs, Stuttgart 1972, (OCLC 246762694)
- 18 Schikore, Jonas: Rendering of the Kinetic Umbrella, in: Kinetic Umbrella
- 19 Schikore, Jonas: Sequence of the umbrella opening and closing, in: Kinetic Umbrella
- 20 Sun, Tao; Lindner, Clemens: Form change of rhombus
- 21 Sun, Tao; Lindner, Clemens: Form change of test model
- 22 Sun, Tao; Lindner, Clemens: Sketch: shingles, two points
- 23 Sun, Tao; Lindner, Clemens: Photo: shingles, two points
- 24 Sun, Tao; Lindner, Clemens: Sketch: shingles, one point
- 25 Sun, Tao; Lindner, Clemens: Photo: shinales, one point 26 Sun, Tao; Lindner, Clemens: Sketch: sliding, parallel

sliding, parallel

mechanical bunching

mechanical bunching

folding origami

folding, origami

folding, fan shaped

33 Sun, Tao; Lindner, Clemens: Photo: folding, fan shaped

cable, linear

cable, linear

cable, cross-module. 37 Sun, Tao; Lindner, Clemens: Photo:

curved folding I

curved folding I

curved folding II

curved folding II

curved folding III

- 44 Sun, Tao; Lindner, Clemens: Overview of different cladding systems
- 45 Sun, Tao; Lindner, Clemens: Parameter overview

comparison

positions methods

- 27 Sun, Tao; Lindner, Clemens: Photo:
- 28 Sun, Tao; Lindner, Clemens: Sketch:
- 29 Sun, Tao; Lindner, Clemens: Photo:
- 30 Sun, Tao; Lindner, Clemens: Sketch:
- 31 Sun, Tao; Lindner, Clemens: Photo:
- 32 Sun, Tao; Lindner, Clemens: Sketch:
- 34 Sun, Tao; Lindner, Clemens: Sketch:
- 35 Sun, Tao; Lindner, Clemens: Photo:
- 36 Sun. Tao: Lindner. Clemens: Sketch:
 - cable cross-module
- 38 Sun, Tao; Lindner, Clemens: Sketch:
- 39 Sun, Tao; Lindner, Clemens: Photo:
- 40 Sun, Tao; Lindner, Clemens: Sketch:
- 41 Sun, Tao; Lindner, Clemens: Photo:
- 42 Sun, Tao; Lindner, Clemens: Sketch:
- 43 Sun, Tao; Lindner, Clemens: Photo: curved folding III
- 46 Sun, Tao; Lindner, Clemens: Orientation
- 47 Sun, Tao; Lindner, Clemens: Mounting
- 48 Sun, Tao; Lindner, Clemens: Mounting

- 49 Sun, Tao; Lindner, Clemens: Pattern / colour study using water colour
- 50 Sun, Tao; Lindner, Clemens: Pattern / colour study on the 1:3 model cut-out
- 51 Sun, Tao; Lindner, Clemens: Valid profile lenath
- 52 Sun, Tao; Lindner, Clemens: Sketch showing the gap issue
- 53 Sun, Tao; Lindner, Clemens: Stripe-wise fixation
- 54 Sun, Tao; Lindner, Clemens: Unit-wise fixation
- 55 Sun, Tao; Lindner, Clemens: Stripe-wise length comparison
- 56 Sun, Tao; Lindner, Clemens: Unit-wise length comparison
- 57 Sun, Tao; Lindner, Clemens: Cull pattern diagram
- 58 Sun, Tao; Lindner, Clemens: Tolerance issue
- 59 Sun, Tao; Lindner, Clemens: Cull pattern
- 60 Sun, Tao; Lindner, Clemens: Isometric view of the resulting design
- 61 Sun, Tao; Lindner, Clemens: Cable groups and the individual lengths
- 62 Sun, Tao; Lindner, Clemens: Laser-cut test profiles
- 63 Sun, Tao; Lindner, Clemens: Milled test profiles
- 64 Sun, Tao; Lindner, Clemens: Milling process
- 65 Sun, Tao; Lindner, Clemens: Elevation of 1:1 model cut-out
- 66 Sun, Tao; Lindner, Clemens: Profile test model
- 67 Sun. Tao: Lindner. Clemens: Mounting detail of profile
- 68 Sun, Tao; Lindner, Clemens: Colour test
- 69 Sun, Tao; Lindner, Clemens: Cable overview
- 70 Sun, Tao; Lindner, Clemens: Cable close-up view

- 71 Sun, Tao; Lindner, Clemens: Elasticity test
- 72 Sun, Tao; Lindner, Clemens: Form change of 1:1 model cut-out
- 73 Sun, Tao; Lindner, Clemens: Colourisation on the 1:1 model cut-out
- 74 Jeongmoon Choi: LINESCAPE
- **75** Sun, Tao; Lindner, Clemens: Top view 1:3 model, open
- **76** Sun, Tao; Lindner, Clemens: Front view 1:3 model, open
- 77 Sun, Tao; Lindner, Clemens: Top view 1:3 model, closed
- 78 Sun, Tao; Lindner, Clemens: Front view 1:3 model, closed

Acknowledgement

We would like to say a big thank you to Jonas Schikore for making this work possible as part of his dissertation and for his constant support throughout the semester. We really appreciate this unique mentoring and had tremendous joy developing and realising the project.

Many thanks also go to Prof. Eike Schling (University of Hong Kong) and Prof. Pierluigi D'Acunto (Technical University Munich), who were always available for us and helped us a lot with valuable feedback and professional input.

Furthermore, we would like to thank the company Gepotex for their competent consultation in the field of textiles and their generous sponsoring, which made the realisation of the work possible.

Many thanks also go to the workshop of the Faculty of Architecture of the Technical University Munich, who advised us at all times with their technical know-how.

Transformable Cladding Systems

This thesis is about the cladding systems of transformable structrues, and is divided into three parts.

The first part gives comprehensive background information to understand the current relevance of the work and its context.

In the second part (design), numerous studies on different systems of cladding are explored. In particular, systems are designed based on the Kinetic Umbrella, a research project of the Technical Universty Munich, Germany. Using an architectural iterative design process, geometric constraints and project specific factors, a cladding system is designed.

In the third part, the fabrication, a detailed design of the cladding system is carried out in order to be able to realise it with the help of digital fabrication.

Following this, the potentials and weaknesses of this design with regard to transformable cladding systems are assessed and an analysis will be created by constructing a 1:3 model of the Kinetic Umbrella.