VCSEL-Based Atmospheric Trace Gas Sensor Using First Harmonic Detection

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Abstract—This paper presents a measurement system based on the first harmonic in tunable diode laser absorption spectroscopy using a vertical-cavity surface-emitting laser to measure the atmospheric CO₂ and H₂O concentrations. The developed system separates the residual amplitude modulation signal from the harmonics and then eliminates it. A digital signal processing is developed to autonomously infer the wavelength and light intensities of the laser. The gas concentrations are determined without extra calibration. The long-term measurements are taken to validate the precision and accuracy of the system. Based on the Allan variance analysis, the broad wavelength scanning enhances the measurement precision, and the first-harmonic detection can achieve about two times as high precision as the traditional second-harmonic detection. The field measurements implemented in early spring of 2018 in Munich were compared with the commercial nondispersive infrared (NDIR) sensor. The outcomes have revealed that our system has high accuracy for the gas concentration measurements and high consistency with the NDIR sensor. The diurnal variations of CO₂ concentration have demonstrated that CO2 concentration in urban areas is affected by the biosphere and meteorological conditions and the daily anthropogenic activities. Furthermore, the air trajectory analysis based on the HYSPLIT model has found that the CO₂ emission sources primarily come from the southeast of Munich. The developed system described in this paper has a great potential for in situ trace gas concentration measurements, the analysis on the polluted gas distributions, and the verification of the pollutant transport model in urban areas.

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Index Terms—Trace gas concentration, tunable diode laser absorption spectroscopy (TDLAS), wavelength modulation spectroscopy (WMS), first harmonic, vertical-cavity surface-emitting laser (VCSEL).

I. INTRODUCTION

REENHOUSE gases (GHG) have a significant negative impact on the climate change. Research has indicated that carbon dioxide (CO₂), one of the dominant GHG, has

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increased by about 2 ppm (parts per million) per year in recent years. The cities and their surroundings sustain around 54% of the global population and contribute nearly 70% of the total anthropogenic CO_2 emissions [1]. Therefore, continuously measuring the CO_2 concentration is of great significance for controlling the carbon emissions and studying the diffusion of the pollutant in urban areas [2]–[4].

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Tunable diode laser absorption spectroscopy (TDLAS) is a typical method for the in-situ trace gas measurements since the laser scans across the absorption line at an extremely small bandwidth, around 30 MHz or smaller, which is about one-tenth of the absorption linewidth [5]–[7]. Unlike the direct TDLAS is employed when absorbance is above 1%. the wavelength modulation spectroscopy (WMS) has wide applications in the trace gas measurements (absorbance less than 1%) and the harsh environments [8], [9]. The theory and mathematical definitions of WMS are outlined in Appendix A. However, due to the arbitrary variation in the phase shift in wavelength, the concentration-dependent harmonics are assigned to X and Y axes in the lock-in amplifier (LIA) at random. Hence, to obtain the complete harmonics, the most common methods are either manually setting the phase of reference signal or using the magnitude of two axes. The former method is inconvenient, while the latter is widely employed in applications [10]. The phase shift in wavelength is discussed in Appendix A.

The harmonics produced by the LIA consist of the absorption line shape and gas parameters information [11], [12]. The concentration-independent residual amplitude modulation (RAM) deforms the harmonics especially the first harmonic. In the well-known "calibration-free nf/1f" method, the RAM in the first harmonic is used to normalize the other harmonics [13]–[15]. Nevertheless, the RAM is acquired from the absorption-free condition, it should be characterized carefully prior to the measurement or from a separate laser beam which makes the measurement inconvenient and complex [10]. Additionally, W. Johnstone et al. used the RAM to recover the absorption line shape based on the phasor decomposition method. However, this method is valid under small modulation index (m < 0.5) when only the first harmonic is utilized, which leads to low harmonic signal-to-noise ratio (SNR); nonetheless, it can be used for any m values if the tuning coefficient is given and higher harmonics are employed [16]–[19]. An external optical fiber and the balanced detection were applied to null RAM in the intensity modulated experiment, which increased the complexity in operation and signal

processing [20]–[22]. Hangauer *et al.* [11] utilized multi-harmonic to reconstruct the transmission and Peng et al. [23] employed odd-harmonic to recover the absorbance shape, the m was extended to higher values (m > 2.0) in their approaches.

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Compared with the conventional distributedfeedback (DFB) laser, the vertical-cavity surface-emitting laser (VCSEL) has many unique features, such as low power consumption, fast and wide wavelength tuning range to cover several absorption lines. Thus, the wide tuning VCSEL can be used to simultaneously measure different gases [24]-[27]. The first harmonic has the highest SNR among all harmonics, thus, theoretically it should have a highest precision in gas sensing. However, due to the strong RAM, the first harmonic is distinctly deformed as a non-linear offset with a gradient particularly in the wide tuning situations (see black line in Fig. 4(b)). Therefore, the magnitude of X and Y components in the first harmonic cannot be employed directly to infer the gas concentration. It is crucial to build up a simple system and eliminate the RAM in the continuous gas measurement when using the first harmonic detection.

In J. Chen and A. Hangauer's research, the broad scanning range was employed for the wavelength calibration while the narrow scanning was for gas concentration measurements using the linear least square curve fitting (LLSCF) algorithm [28], [29]. They concluded that the second harmonic detection had higher precision than the first harmonic detection [11]. On the contrary, Lan *et al.* [30] focused on using the wide tuning VCSEL multi-harmonic for gas concentration measurement and found that the first harmonic could achieve better performance than the second harmonic in gas detection. It has shown that multi-harmonic detection including first harmonic can enhance the precision of the system. However, the previous study did not focus on the removal of RAM in first harmonic and the development of a compact system using first harmonic for urban GHG measurements.

This article focuses on utilizing the first harmonic for atmospheric gas sensing based on the VCSEL's wide tuning range. A measurement system was developed to autonomously eliminate the RAM signal in the harmonics, calibrate the wavelength and laser light intensities, and measure the *in-situ* CO₂ and H₂O concentrations. Then, Allan-Werle Variance Analysis was deployed to analyze the precision of our measurement system. The field measurement compared with the commercial nondispersive infrared (NDIR) sensor was carried out in early spring of 2018 in Munich. The analysis on the CO₂ diurnal variation demonstrated that the CO₂ concentration in urban areas is affected not only by biosphere and meteorological conditions but also by the daily anthropogenic activities. The backward trajectory analysis based on HYSPLIT model was implemented to identify CO₂ sources in urban areas.

II. EXPERIMENTAL FOUNDATION

A. First Harmonic Detection

The basic principle of WMS has been introduced in several articles [11], [12], [31]. According to Eqs. 6 and 8 in Appendix A, for optically thin samples (absorbance $\ll 10\%$), $A_0 \approx 1$ and $A_1, A_2, A_3, A_4, \cdots \ll A_0$, which are assumed as 0. Thus,

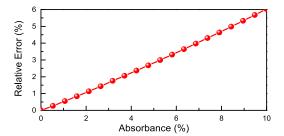


Fig. 1. The error analysis of concentration measurement when the S_{0f} is served as $S_{0f} \approx \overline{I_0}$ to normalize the harmonics.

the zeroth harmonic picked out via LIA is: $S_{0f} = I_{0\theta}^X \approx \overline{I_0}$. The S_{0f} can be served as the central light intensity $(\overline{I_0})$ when the absorbance is weak [32].

When normalized with respect to S_{0f} , the X and Y components of first harmonic, X_{1f} and Y_{1f} , are simplified as:

$$\begin{cases} X_{1f} = A_1 + \frac{I_1}{\overline{I_0}} \cos \psi \\ Y_{1f} = \frac{I_1}{\overline{I_0}} \sin \psi. \end{cases}$$
 (1)

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It can be learned from Eq. 1 that X_{1f} consists of two parts: the harmonic signal (A_1) , which includes gas parameters, and the cosine ψ of RAM; while Y_{1f} is concentration-independent and only contains the sine ψ of RAM. The ψ can be determined when Y_{1f} , $\overline{I_0}$ and I_1 are given. Then, the measured ψ is employed to eliminate RAM when it is substituted into the X_{1f} expression:

$$\overline{X_{1f}} = X_{1f} - \frac{Y_{1f}}{\tan \psi} = A_1 = PS(T)LcH_1,$$
 (2)

where H_1 are the first order Fourier components of the spectral line shape. Thus, the $\overline{X_{1f}}$ is pure concentration-dependent and can be used to infer gas concentration when P and T are given:

$$c = \frac{\overline{X_{1f}}}{PS(T)LH_1}. (3)$$

From Eq. 3, the gas concentration can be obtained without the extra calibration against the standard reference gas. Thus, this method gets rid of the calibration proces.

Figure 1 is the error analysis of the concentration measurement when S_{0f} is used as $\overline{I_0}$ to normalize the harmonic signals. As can be seen from Fig. 1, the relative errors increase as the increment of the absorbance. To ensure the measurement error within 1%, the absorbance should not exceed 2%. Therefore, for the trace gas measurement when absorbance $\ll 10\%$, the approximation of $S_{0f} \approx \overline{I_0}$ will not introduce a large measurement error.

B. Experimental Setup

The diagram of the experimental setup is shown in Fig. 2. A VCSEL (VL-2004-1-SQ-A5) [33] is used as the light source whose wavelength is controlled by a laser driver (Arroyo Instruments 6301). The absorption signal is reflected by a concave mirror with 75 mm of focus length and collected into an InGaAs amplified photodetector (PD, PDA10DT-EC). Subsequently, the detected signal is recorded and digitized

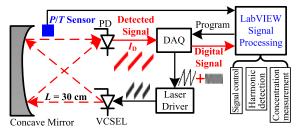


Fig. 2. Experimental setup for trace gas concentration measurement.

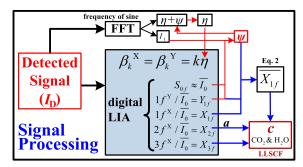


Fig. 3. Signal processing of harmonic detection and gas concentration measurement. The red arrows are the process to determine ψ in an iterative procedure. The shade part is the digital lock-in amplifier (LIA).

via a high-speed memory data acquisition card (DAQ, NI USB-6361, resolution: 16 bits, and sampling rate: 2MS/s). The digitized data is sent into the signal processing to further calculate gas concentration. In this process, the DAQ is deployed not only to record the detected signal but also as a signal generator to provide the ramp and sinusoidal signals such that the laser wavelength is modulated. A sensor using the Raspberry Pi system is set nearby to synchronously measure *P* and *T*. The signal processing is explained in the following Sect. II-C.

C. Autonomous Measurement System

A digital signal processing (LabVIEW) is developed to calculate the intermediate parameters as mentioned in Sect. II-A and Appendix A, and to obtain gas concentrations. The first part of the processing is the signal controlling and acquisition. The LabVIEW programs DAQ to generate the low-frequency ramp (10 Hz, 1.2 V) and high-frequency sinusoidal (6 kHz, 60 mV) signals to modulate the VCSEL in a wide range, and then to record the absorption signal into LabVIEW, which is shown as black line in Fig. 4(a). In this case, the modulation indices (*m*) of each line are around 3.0 which ensures the high SNR of the first, second and third harmonics (Fig. 5, Appendex B).

The second part is the harmonic detection. As indicated in Fig. 3, a digital LIA is developed to produce the zeroth to third harmonics. Note that the zeroth harmonic can be produced in our developed LIA by setting the frequency of the reference signal to 0. The red dotted line in Fig. 4(a) is the central light intensity $(\overline{I_0})$. In WMS, the zeroth harmonic (S_{0f}) can be treated as: $S_{0f} \approx \overline{I_0}$ when the absorbance is weak (absorbance $\ll 10\%$). The S_{0f} is averaged from the 10 sequential scans (10 Hz) to improve SNR and used to normalize the other harmonics. Figure 4(b) exhibits the curves of the normalized X_{1f} and Y_{1f} . The peak positions of each absorption lines (the

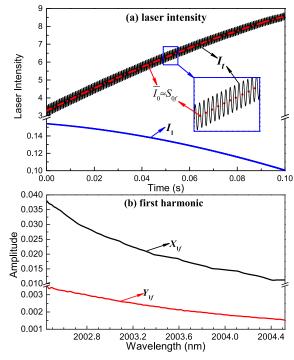


Fig. 4. (a) The detected signal via the photodetector (I_t) and its central light intensity $(\overline{I_0})$, red dotted line). The S_{0f} can be served as $S_{0f} \approx \overline{I_0}$ when the absorbance is weak. The modulation intensity (I_1) is obtained from an FFT subroutine. (b) The normalized X and Y components of first harmonic in a scanning cycle, where X_{1f} includes the RAM.

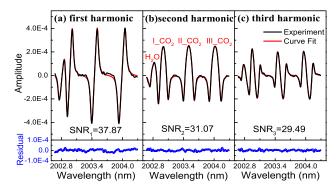


Fig. 5. Wide-scanned concentration-dependent harmonic signals obtained from Fig. 4(a); (a) first harmonic without RAM, (b) second harmonic, and (c) third harmonic. The red lines are the calculation curves based on the LLSCF. The bottoms are the residuals of curve fit results. The concentrations of CO₂ and H₂O are 411.8 ppm and 5.56%, respectively.

absorption line centers are 2002.829 nm (H_2O), 2002.998 nm, 2003.503 nm, and 2004.019 nm, respectively) in the normalized X_{2f} (Fig. 5(b)) are picked as the absorption line centers, thus, the wavelength versus the ramp signal is calibrated and the modulation depths (a) are determined (Appendix C). A Fast Fourier Transform (FFT) subroutine is established to measure the modulation intensity (I_1 , as blue line in Fig. 4(a)) and light intensity phase ($\eta + \psi$) when the extracted frequency is set the same as sine signal (6 kHz). An iterative procedure is created to determine the phase shift (ψ) as follows: a very first $\psi_1 = 0^\circ$ is used to subtract ψ in the phase ($\eta + \psi$) and get η_1 . Then, the phase of the reference signal is set as $\beta_1^Y = \eta_1$ to receive Y_{1f} . Afterwards, according to $\overline{I_0}$, I_1 and Y_{1f} , a new ψ_2 is obtained. The process is reiterated until ψ is constant. In our system, when the sine frequency is 6 kHz, $\psi = 6.7^\circ$.

Thereby, when given $\overline{I_0}$, I_1 , ψ , and η , the X_{kf} and Y_{kf} are obtained by setting the reference phase signal to: $\beta_k^{\rm X} = \beta_k^{\rm Y} = k\eta$ (see Appendix A). The concentration-dependent $\overline{X_{1f}}$ is acquired according to Eq. 2.

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In the third part, the harmonics with different scanning ranges are extracted to infer gas concentrations based on the LLSCF algorithm [34], [35]. The spectral parameters of the absorption lines are acquired from the HITRAN databases and utilized for calculating H_k [36]. The curve fitting results of the first, second and third harmonics with three CO₂ absorption lines and one H₂O absorption line are displayed in Fig. 5. The residuals in the bottom are in an order of 1×10^{-5} , indicating the high accuracy of the system.

Throughout the process, the wavelength and light intensities, and the harmonics are autonomously calibrated in the absence of the standard optical components such as etalon, beam splitter, and the absorption-free laser path. The entire procedure takes about 0.5s which enables the real-time measurement. As Eq. 3 demonstrates, the gas concentrations are obtained without the standard reference gas. Therefore, this system is an autonomous calibration system for in-situ trace gas measurements. The absorbance of about 2% for the GHG sensing ensures that the assumption of $S_{0f} \approx I_0$ is valid in the system. The P and T compensations are carried out in the measurements. The air-broadening is dominant while the self-broadening uncertainty (<1%) can be ignored in Pressure Broadening in the trace gas measurements [15]. Furthermore, the $\overline{I_0}$ is on-the-fly measured in every scanning cycle, the fluctuations of the light intensity can be instantaneously eliminated during the measurement. This system thus can be utilized even in vibration situations where the laser path is difficult to fix.

Using VCSEL, the wide tuning range which covers several gas species in a cycle enables not only the wavelength calibration but also several gas concentrations to be measured simultaneously. From Fig. 5, the first harmonic without RAM has the highest magnitude and highest SNR of 37.87, meaning that it has the best noise performance among all harmonics. However, compared the black line in Fig. 4(b) and the curves in Fig. 5(a), which included and excluded the RAM, the RAM in the original first harmonic is a distinct non-linear offset with gradient that submerges the harmonic signal. The RAM is complicated and difficult to determine in the wide tuning VCSEL. Consequently, it is important for VCSEL to eliminate RAM in the wide tuning range for first harmonic detection. Furthermore, the second order modulation intensity (I_2) is much smaller than I_1 (0.3% of I_1) so that the RAM in the second harmonic can be treated as a slope and an offset, as presented in [29]. The higher order modulation intensities can be neglected since they are even smaller.

III. EXPERIMENTAL RESULT AND ANALYSIS

A. Allan-Werle Variance Analysis

Allan-Werle Variance is a method to identify and quantify the different noise terms that exist in the inertial sensor data, and calculate the detection limit of the sensor in the time domain [37], [38]. As displayed in Fig. 6, when the Allan Deviation (σ_{Allan}) is minimum (σ_{Allan}^{min}), the optimum integrating time (τ_{opt}) and the detection limit are determined. Allan

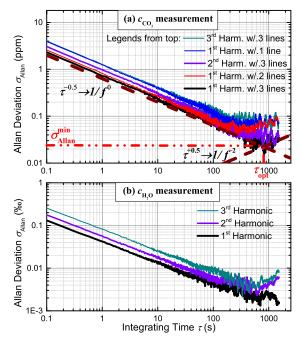


Fig. 6. Allan Deviations of the first, second and third harmonics with different absorption lines for CO_2 and H_2O concentration measurements. The winered lines represent slopes of -0.5 and 0.5, which correspond to the power densities $S(f) = f^0$ (white noise) and $S(f) = f^{-2}$ (Brownian noise), respectively.

Gas	S_{nf} w/. lines	$\sigma_{ m Allan}$ @1s	$\sigma_{ m Allan}$ @ 1 min	$\sigma_{\mathrm{Allan}}^{\mathrm{min}} @ au_{\mathrm{opt}}(\mathbf{s})$
	1 st w/. 1	1.24ppm	0.16ppm	0.07ppm@300
	1 st w/. 2	0.81ppm	0.11ppm	0.06ppm@300
CO ₂	1 st w/. 3	0.72ppm	0.10ppm	0.027ppm@800
2	2 nd w/. 3	0.97ppm	0.12ppm	0.05ppm@400
	3 rd w/. 3	1.27ppm	0.18ppm	0.09ppm@200
	1 st w/. 1	0.042%	$0.006\%_{o}$	0.002‰@600
H_2O	2 nd w/. 1	0.057%e	$0.007\%_{o}$	0.004%e@400
	3 rd w/. 1	$0.082\%_{o}$	$0.011\%_{o}$	0.005%@200

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Deviations for CO₂ and H₂O concentration measurements are demonstrated in Fig. 6 and Table I. The measurement is performed in a stable climate chamber with the surrounding conditions of temperature: 296 ± 0.5 K and pressure: $0.95 \pm$ 0.01 atm, and CO₂ and H₂O concentrations of 466.8 \pm 0.2 ppm and $5.05 \pm 0.01\%$, respectively. From Fig. 6(a), the plots of the first harmonic detection illustrate that the more absorption lines are included, the higher precise the measurement is. That is, compared with the measurement result of the single absorption line (II_CO₂, as annotated in Fig. 5(b)), the first harmonic detection with double (II and III CO₂) and triple absorption lines (I, II and III_CO2) have lower deviations. For example, the σ_{Allan} of the double and the three absorption lines are 0.81 ppm and 0.72 ppm with 1s averaged, respectively; while the σ_{Allan} of the single line is 1.24 ppm. It concludes that the first harmonic detection with extended scanning range can improve the measurement precision.

When the RAM effect is eliminated, the first harmonic detection has higher precision than that of the second and third harmonic detections. That is, the Allan plots of the first harmonic have lower white and Brownian noise levels during the entire integrating time. Taking the H₂O measurement as

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an example, the first harmonic achieves $6 \times 10^{-3}\%$ of the deviation with 1min averaged, while the second and the third harmonic detections only obtain $7 \times 10^{-3}\%$ and 0.011% with the same integrating time, respectively. In terms of the detection limits, the first harmonic with three absorption lines obtains 0.027 ppm when the τ_{opt} is 800s for CO₂ concentration measurement, while the $\sigma_{\rm Allan}^{\rm min}$ of the second harmonic is only 0.05 ppm with 400s averaged. In H₂O detection, the $\sigma_{\text{Allan}}^{\text{min}}$ of the first harmonic is $2 \times 10^{-3}\%$ with 600s averaged, while the σ_{Allan}^{min} of the second harmonic is $4 \times 10^{-3}\%$ with 400s averaged. That is to say, the first harmonic detection has about two times better precision than the traditional second harmonic detection. As shown in Fig. 4(b), the primitive first harmonic curve is deformed in the wide scanning range because of the existence of the RAM. The harmonic signal is even submerged in the RAM and is hard to use for the concentration measurement. However, when the RAM signal is removed, the first harmonic detection has the best performance among all harmonics. Therefore, the elimination of RAM in the first harmonic is necessary and can effectively improve precision in gas sensing.

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In short, the Allan Deviation Analysis demonstrates that when the RAM signal has been eliminated, the first harmonic detection has the highest precision in the gas concentration measurement. It can enhance the precision by nearly double when compared with the traditional second harmonic detection. That is because the first harmonic signal has the largest magnitude and SNR among all harmonics. As shown in Fig. 5, the SNR of the first harmonic is 37.87 which is higher than the second harmonic (31.07). The higher the order of the harmonic is, the lower the amplitudes and SNR are. Therefore, the low-order harmonics can achieve better precision performance in measurement. Widening the scanning range can not only measure various gas species simultaneously, but also can obtain higher precision because more information in the absorption lines are utilized. The experimental results also indicate the high stability of the measurement system.

B. Accuracy of the Measurement

The comparison experiments are implemented to verify the accuracy of our developed system, where a commercial NDIR sensor (Li-Cor 840A CO_2/H_2O gas analyzer) is served as a standard instrument as in [30]. However, due to the frequency instability of the optical filter which is controlled by the piezo, the NDIR sensor must be calibrated periodically according to the application and utilization frequency [39]. The inlet gas tube of the NDIR sensor is set close to the optical path of the TDLAS system. These two sensors are operated separately and simultaneously to acquire CO_2 and H_2O concentrations.

Figure 7 illustrates the comparison results of CO_2 and H_2O concentrations dating from March 30 to April 11, 2018. The outcomes of TDLAS are retrieved from the first harmonic detection with 10 min averaged for which the σ_{Allan} are 0.03 ppm for CO_2 concentration and 0.02‰ for H_2O concentration, as illustrated in Fig. 6 and Table I. From Fig. 7, we can learn that the measured concentrations from the TDLAS system is closely aligned with the values measured by the NDIR sensor, which reveals that these two sensors have a high consistency with each other. As shown in the

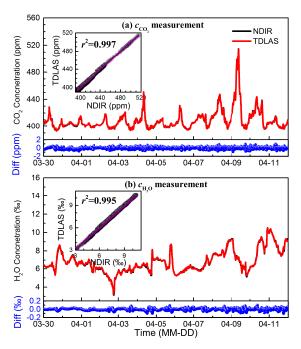


Fig. 7. CO₂ and H₂O concentrations measured by TDLAS and NDIR sensors, the experimental data is averaged over 10 minutes.

bottom of the plots, the differences between these two sensors are less than 1 ppm for CO₂ concentration and 0.1% for H₂O concentration (much less than 1% relative), indicating the high accuracy of the developed system. Moreover, the linear regressions between the TDLAS and NDIR sensors are also demonstrated in Fig. 7, where the regression ranges are 390–520 ppm with absorbance of $1.6 \times 10^{-3} - 2.1 \times 10^{-3}$ for CO₂ and 3–11% with absorbance of $5 \times 10^{-4} - 1.8 \times 10^{-3}$ for H₂O, respectively. The correlation coefficients (r^2) of above 0.99 demonstrate the high coherence of the two systems.

Overall, the wide scanning first harmonic signal can be utilized for measuring CO₂ and H₂O concentrations when the RAM is eliminated. The experimental results have confirmed that the first harmonic detection has high accuracy in gas sensing and has high consistency with the NDIR sensor. Furthermore, compared with the multi-harmonic detection, the sole first harmonic detection achieves a more stable measurement because less information is employed in the signal processing. The results have indicated that the first harmonic detection is more favorable in data processing and has wider applications in real-time GHG measurement [30].

C. Diurnal Variation Analysis

To provide a better understanding about the CO₂ concentration variation in urban areas, the measurement results depicted in Fig. 7 are separated over days and presented in Fig. 8, where the foggy days from April 8 through 10 are excluded in the discussion. During the measurement period, the forsythia was blooming, meaning that most of the plant leaves had just started sprouting and that the vegetation photosynthesis and respiration from the biosphere were still not very strong. As displayed in Fig. 8(a), the diurnal cycle is clearly discernible. However, compared with the daily cycles in our previous work in [30], the lowest CO₂ concentration in the study period

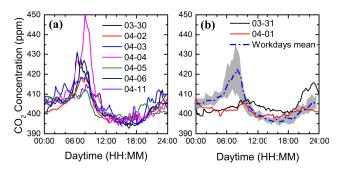


Fig. 8. Daily analysis of the CO₂ concentration measurement in (a) workdays and (b) weekends; the dash-dotted line in (b) is the averaged value of (a), the gray part displays the 68% confidence interval.

(395 ppm) is higher than that in September (380 ppm) but lower than that in December (above 400 ppm). That is because the photosynthesis in early spring is weaker than that in September but stronger than that in December in Munich. Moreover, the averaged atmospheric temperature during the study period (about 8 °C) is lower than in September (15 °C) but higher than in December (0 °C), leading to the height of the planetary boundary layer (PBL) stay between the heights of these two months. The sun heats up the ground surface in the day, thus the PBL increases while the CO₂ concentration decreases. At night, the opposite occurs: the drop of the PBL increases the CO₂ concentration [40].

The ground-based CO₂ concentration is also influenced by the anthropogenic activities. Compared with the data measured on weekends, peak curves can be found in the morning from 06:00 to 10:00 on the workdays in Fig. 8(a). This is likely caused by rush-hour traffic increases between these hours, which results in increasing the CO₂ concentration. On the weekends, when the weather was fair, there was no rush-hour peak at these hours, as can be seen in Fig. 8(b) [41]. This phenomenon indicates that the human activities have a great influence on the CO₂ concentration in urban areas. Not only the special events like the festival celebrations in our previous study, but also the daily activities have a noticeable influence on the air quality in urban areas [30]. The above analysis demonstrates that the diurnal variation of CO2 concentration in urban areas is an integrative role combining the vegetation photosynthesis and respiration, the PBL (atmospheric temperature), and the daily anthropogenic activities of that area.

D. Air Trajectory Analysis

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Nowadays, combining measurements with simulations is a conventional way to study and control carbon emissions in urban areas. The HYSPLIT (Hybrid Single Particle Lagrangian Integrated Trajectory) model is a common method to establish locations of emission sources from the receptor site [42]. Combined with the measured gas concentration at the time when the air parcel arrives at the measurement site, the air backward trajectories depict the air movement and gas distribution on the calculated paths. The PSCF (Potential Source Contribution Function) calculates the probability that describes the spatial distribution of probable source locations. The PSCF value is given as: $PSCF = m_{ij}/n_{ij}$ in which n_{ij} is the total number of trajectories that pass through the cell (i, j) and m_{ij} is the number of trajectories resulting in gas concentration

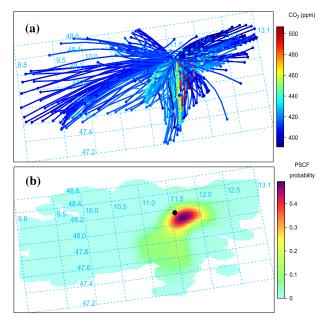


Fig. 9. (a) Six-hour backward air trajectories combined with the measured CO_2 concentration (Fig. 7). (b) PSCF plot with over 75^{th} percentile (CO_2 : 420 ppm); the black circle is the measurement site.

that greater than a specific threshold (75^{th} percentile of CO_2 concentration in the study, 420 ppm) [43], [44].

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As illustrated in Fig. 9, the backward trajectories are calculated hourly combined with CO₂ concentration ending at the measurement site (receptor) (48.151° N latitude and 11.568° E longitude) during the whole measurement period (Fig. 7) and then processed by the Openair package in R [45]. Six-hour backward trajectories are selected because the time is sufficient to determine the probable locations of both local and regional sources in urban areas [46]. The trajectories are divided into $0.05^{\circ} \times 0.05^{\circ}$ cells and the PSCF plot is smoothed as shown in Fig. 9(b), where the black circle is the position of the measurement site located at Munich. The cells are colored according to the PSCF values, with the dark-red part illustrating the highest probability of the source location. The measurement site is in the north of Munich city center, where the Munich Central Station, the Old Town and shopping malls locate at its southeast and are within a radius of 5 km.

As indicated in Fig. 9(a), the air mass was primarily from the east, south and west directions, and few occurrence of air was from the north during the study period. The air from the south direction was much more polluted than that from east and west. From Fig. 9(b), we can learn that the darkest part is in the southeast of the measurement site, demonstrating the main emission source from this area in the period, which corresponds to the district with a high population density and high CO₂ emissions. The preliminary air trajectory analysis has exhibited that when combined with the air trajectory model, the measurement results can be used for emission assessment. Therefore, our developed system can be applied in studying the CO₂ distribution and predicting the pollutant emission sources in urban areas.

IV. CONCLUSION

In conclusion, this paper developed a measurement system to autonomously eliminate the RAM in the first harmonic,

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and measure the gas concentrations using the broad scanning range VCSEL. At first, the method of first harmonic detection was proposed. Then, a digital signal processing pipeline was introduced to autonomously eliminate the RAM, calibrate the wavelength and light intensities, and infer gas concentrations. Subsequently, the CO₂ and H₂O measurements were implemented in both the stable environment and the field areas to verify the precision and accuracy of the developed system. According to the Allan-Werle Variance Analysis, widening the wavelength tuning range can enhance the precision of the developed system. The precision of the first harmonic detection was nearly doubled compared with the traditional second harmonic detection. The field measurements carried out in early spring of 2018 in Munich were compared with the commercial NDIR sensor. The results indicated that our developed system displayed high accuracy and had high consistency with the NDIR sensor. Further analysis revealed that the diurnal variations of the atmospheric CO₂ concentration in urban areas are the comprehensive combination of the biosphere and meteorological conditions, and the local daily anthropogenic activities. The backward air trajectories were calculated based on the HYSPLIT model and PSCF method, the preliminarily results have shown that the CO₂ emission sources mainly come from the southeast of Munich. According to the experimental and analysis results, the developed system presented in this article has a great potential for measuring the in-situ GHG concentrations, analyzing the polluted gas distributions, and validating the pollutant transport model in urban areas.

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APPENDIX A THEORY OF WMS

Wavelength modulation spectroscopy (WMS) is a method for sensitive absorbance measurements which uses a significantly faster sinusoidal signal riding on a slowly varying diode laser injection current. Instead of the transmission spectrum, the harmonic signals are obtained via the LIA. Due to its advantages of efficient noise suppression, for example, insusceptible to 1/f noise, WMS enables to increase the sensitivity, precision and SNR in the trace gas measurements and the harsh environments. In TDLAS-WMS, when the laser is tuned by the low-frequency ramp and high-frequency sinusoidal signals, the instantaneous wavenumber and light intensity are expressed as:

$$\begin{cases} v(t) = \overline{v} + a\cos(\omega t + \eta) \\ I_0(t) = \overline{I_0} + I_1\cos(\omega t + \eta + \psi), \end{cases}$$
(4)

where \overline{v} [cm⁻¹] and $\overline{I_0}$ denote the central wavenumber and central light intensity, they are the wavenumber and intensity of the central laser emission (without the sinusoidal modulation) which implemented by the slow ramp signal; a [cm⁻¹] is the modulation depth and the modulation index is $m = a/\gamma$ where γ is the linewidth; I_1 is the modulation intensity; ω [rad/s] is the modulation angular frequency; t [s] is the time; ψ is the phase shift between the wavelength and intensity modulation; and η is the phase shift in wavelength with respect to the tuning current. The η is an arbitrary value in each measurement since the start recording point of the waveform is

unfixed. The light intensity phase is $(\eta + \psi)$ and θ is defined as $\theta = \omega t + \eta$. Based on the Beer-Lambert Law, the transmitted light intensity $(I_D, \text{ detected})$ is:

$$I_{D}(t) = I_{0}(t) \exp[-PS(T)Lc\varphi(v(t))]$$

$$= \sum_{k=0}^{\infty} I_{k\theta}^{X} \cos k\theta - \sum_{k=0}^{\infty} I_{k\theta}^{Y} \sin k\theta, \qquad (5)$$

where P [atm], S(T) [cm⁻²/atm], T [K], L [cm], and c are the total gas pressure, line strength, temperature, absorbing path length, and gas concentration, respectively; φ [cm] is the line shape which is a function of v(t) and can be expressed as a Voigt profile [47]; $I_{k\theta}^{X}$ and $I_{k\theta}^{Y}$ are the k-th ($k = 0, 1, 2, 3, \cdots$) Fourier components of the transmitted light intensity:

$$\begin{cases} I_{0\theta}^{X} = \overline{I_{0}}A_{0} + 0.5I_{1}A_{1}\cos\psi, & I_{0\theta}^{Y} = 0\\ I_{1\theta}^{X} = \overline{I_{0}}A_{1} + I_{1}\cos\psi(A_{0} + 0.5A_{2})\\ I_{1\theta}^{Y} = I_{1}\sin\psi(A_{0} - 0.5A_{2}) & 54\\ I_{k\theta}^{X} = \overline{I_{0}}A_{k} + 0.5I_{1}\cos\psi(A_{k-1} + A_{k+1})\\ I_{k\theta}^{Y} = 0.5I_{1}\sin\psi(A_{k-1} - A_{k+1}), & k = 2, 3, \cdots, \end{cases}$$

$$(6) \quad 54$$

where A_k are the k-th order Fourier components of the transmittance, $A_k = PS(T)LcH_k$ in which the H_k is the k-th order Fourier components of the spectral line shape. In LIA, the k-th Fourier components can be fixed by the same frequency reference signals as:

$$\begin{cases} X: [I_{k\theta}^{X} \cos k\theta - I_{k\theta}^{Y} \sin k\theta] \cos(k\omega t + \beta_{k}^{X}) \\ Y: [I_{k\theta}^{X} \cos k\theta - I_{k\theta}^{Y} \sin k\theta] \sin(k\omega t + \beta_{k}^{Y}), \quad k = 0, 1, 2, \cdots \end{cases}$$
(7) 548

From Eq. 7, it can be seen that the amplitudes of the harmonic in X and Y axes are decided by the relationship between the phase shift in wavelength (η or $k\theta$) and the phases of the reference signal ($\beta_k^{\rm X}$ and $\beta_k^{\rm Y}$). Due to the arbitrary of η , the amplitudes of the harmonic in X and Y axes are variable in each measurement. Generally, the magnitude of the Fourier components is used as the complete harmonic signal: $S_{kf} = \sqrt{I_{k\theta}^{\rm X2} + I_{k\theta}^{\rm Y2}} \approx \overline{I_0} A_k$ when the RAM can be neglected. However, this method is invalid in the first harmonic since the RAM is strong. Or when setting the phases of the reference signal: $\beta_k^{\rm X} = \beta_k^{\rm Y} = k\eta$, the k-th Fourier components can accumulate on their own axes as:

$$\begin{cases} X_{kf} = I_{k\theta}^{X} \\ Y_{kf} = I_{k\theta}^{Y}. \end{cases}$$
 (8)

APPENDIX B MODULATION INDEX

The amplitudes of the first, second and third harmonics vary with the modulation index (m) are calculated as shown in Fig. 10 and Table II, where the gas parameters are the same as Fig. 5. As indicated in the figure and table, when m=2.0 or 2.2, the first and second harmonics would reach to their maximum values while the amplitude of the third harmonic is only 88% of its maximum. When m increases to 3.0, the percentage of the third harmonic will raise to

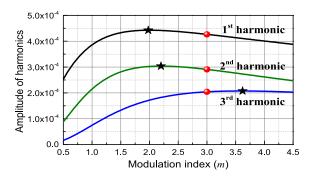


Fig. 10. The amplitudes of the first, second and third harmonics vary with modulation index (m) from 0.5 to 4.5. The black stars denote the maximum at each harmonics and the red dots are the harmonic amplitudes at m = 3.0.

TABLE II

OVERVIEW OF THE HARMONICS AT DIFFERENT MODULATION INDICES, THE PERCENTAGE DATA ARE THE HARMONICS AMPLITUDES COMPARED WITH THEIR OWN MAXIMUM $(m_{\rm MAX})$

	S_{1f}	S_{2f}	S_{3f}
$m_{ m max}$	2.0	2.2	3.6
m=2.2, percent of maximum	99.8%	100%	88.0%
m=3.0, percent of maximum	96.4%	95.8%	98.4%

98.4%, while the amplitudes of the first and second harmonics are still >95% of their maximums. When setting m=3.0, the high SNR harmonics, especially the third harmonic, will be obtained.

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APPENDIX C MODULATION DEPTH

According to Eq. 4, the instantaneous wavenumber can also be expressed as determined by the tuning current (i):

$$v(i) = c_2(i - i_0)^2 + c_1(i - i_0) + c_0,$$
(9)

where i is transferred from the tuning voltage (ramp signal) and the voltage-to-current is determined by the laser controller (5 mA/V in the system); i_0 is the fixed current which can be set as the current at the line centers. The coefficients (c_2 , c_1 , and c_0) can be inferred from the measured line centers. Then, the modulation depth can be calculated by:

$$a = \frac{dv(i)}{di}I_{1}\varsigma(\omega) = [2c_{2}(i - i_{0}) + c_{1}]I_{1}\varsigma(\omega), \quad (10)$$

where $\varsigma(\omega)$ is the frequency dependency of the current-to-wavenumber tuning coefficient, the value can be seen in [29] and [48].

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