

Efficiency of monolithic solvers for incompressible fluid-structure interaction problems



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Motivation

- Real world problems require accurate predictions at reasonable computational costs (accuracy vs. numerical effort)
- Parallel scalability for very large problem sizes

Problem Definition & Discretization

- Solid domain Ω^S : nonlinear elastodynamics
- Fluid domain Ω^F : incompressible Navier-Stokes equations with ALE observer
- Fluid-Structure Interface Γ_{FSI} : weak enforcement of coupling conditions using Lagrange Multiplier field $\lambda = h_{\Gamma_{FSI}}^S - h_{\Gamma_{FSI}}^F$ [1]
- $(\delta\lambda, \underline{d}_{\Gamma_{FSI}}^S - \underline{d}_{\Gamma_{FSI}}^G)_{\Gamma_{FSI}} = 0$ on $\Gamma_{FSI} \times (0, T)$
- Spatial discretization of structure and fluid field with finite elements
- Dual Mortar method for Lagrange multipliers [2] allows for non-matching interface discretization and cheap condensation of Lagrange multipliers.
- Temporal discretization with single-step, single-stage, and fully implicit marching time integrators

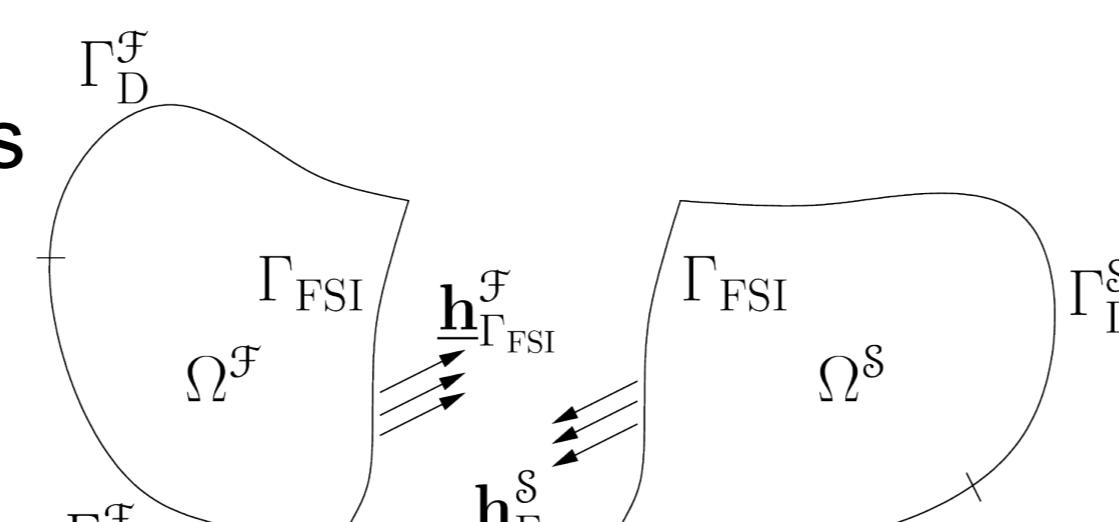


Fig. 1: Problem definition

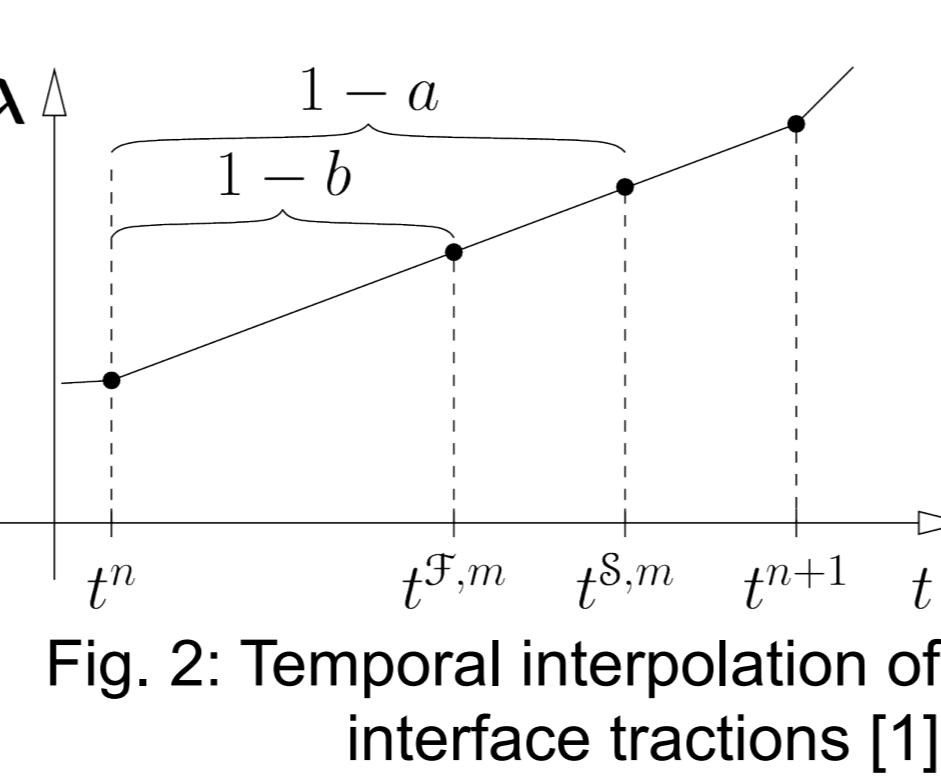


Fig. 2: Temporal interpolation of interface tractions [1]

Adaptive Time Stepping: Algorithm

- Individual error estimation in both fields via
 - Comparison to auxiliary explicit scheme (e.g. Adams-Basforth 2)
 - Zienkiewicz & Xie [3] (structure only)
 - Error norms: length-scaled L2-norms
 - Deduce separate norm for FSI interface DOFs to account for central role of the interface
 - Adapt time step size based on estimated errors
- $$\kappa_{opt} = \left(\frac{\text{tol}}{\text{error}} \right)^{\frac{1}{p+1}}$$
- Compute Δt_{new}^Ω for every subset of DOFs
 - $\Delta t_{new}^\Omega = \min \{ \Delta t_{max}, \max \{ \min \{ \kappa_{max}, \max \{ \kappa_{min}, \kappa_s \kappa_{opt} \} \} \Delta t_{old}, \Delta t_{min} \} \}$
 - Choose minimal time step size suggestion to guarantee accuracy everywhere in the domain
- $$\Delta t_{new} = \min (\Delta t_{new}^\Omega)$$

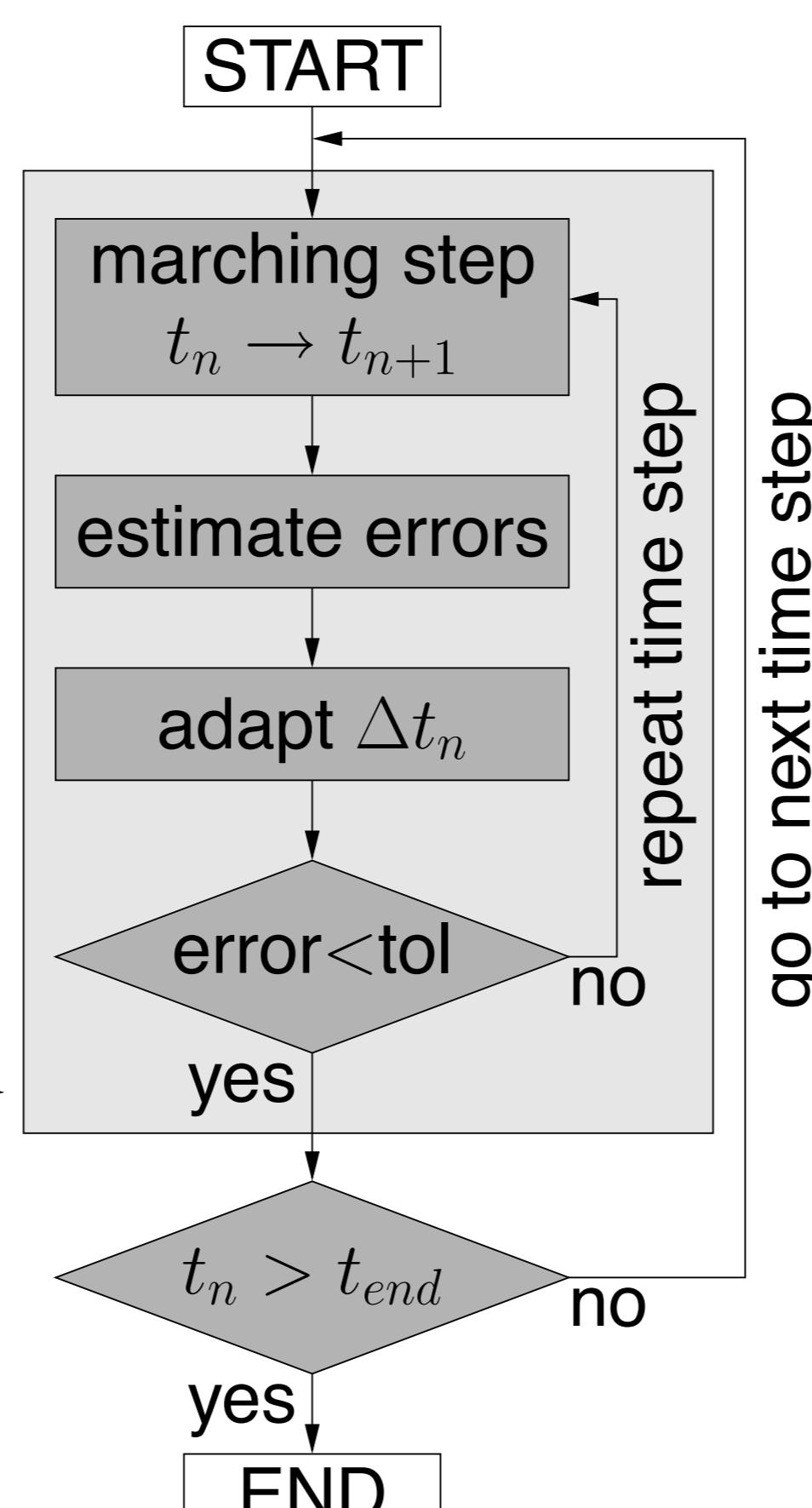


Fig. 3: Adaptive time stepping loop

Newton-Krylov with FSI-specific Preconditioning [4]

Algorithm

- Algebraic coarse level problem

$$A_{k+1}^{FSI} = \begin{bmatrix} R_k^S & R_k^G & R_k^F \\ F_{FS} & G & G_{GF} \\ F_{FG} & F & \end{bmatrix}_k \begin{bmatrix} P_k^S & P_k^G & P_k^F \\ P_k^G & P_k^F & \end{bmatrix}$$

$$= \begin{bmatrix} R_k^S S_k P_k^S & R_k^G G_k P_k^G & R_k^F F_k P_k^F \\ R_k^G G_k P_k^G & R_k^F F_k P_k^F & R_k^F F_k P_k^F \\ R_k^F F_k P_k^F & R_k^F F_k P_k^F & R_k^F F_k P_k^F \end{bmatrix}$$

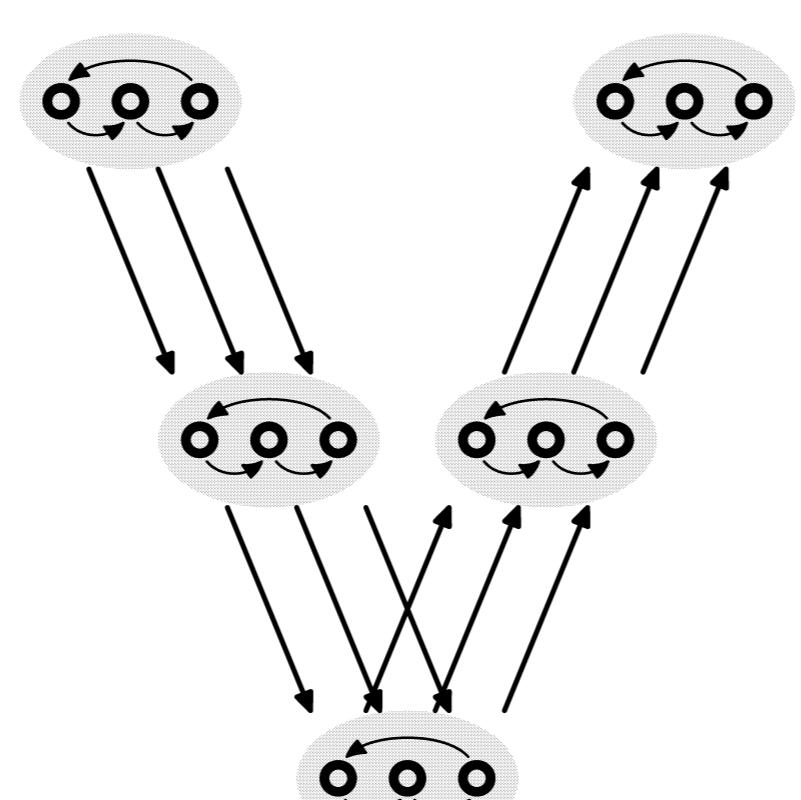


Fig. 6: FSI-AMG V-Cycle for AMG(BGS/Schur) [4]

- FSI coupling on all levels

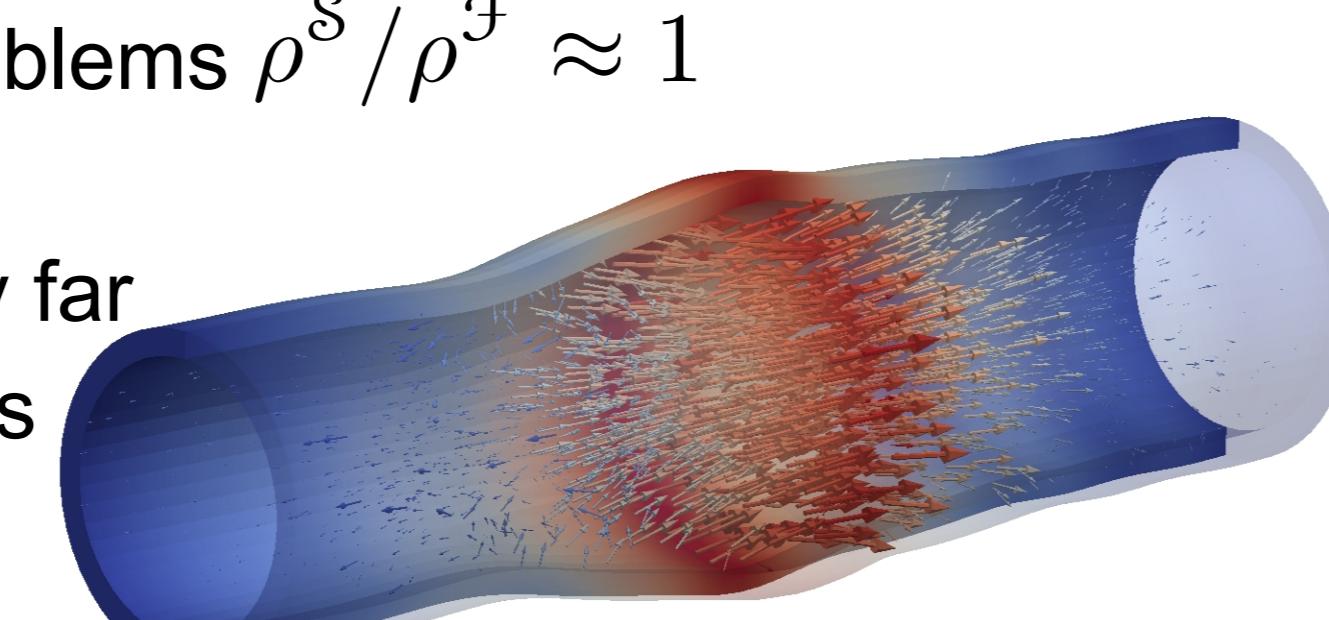


Fig. 7: Solution of pressure wave

AMG(BGS) characteristics averaged over timesteps				
n_{ele}	Newton	GMRES	time	n_{proc}
16	2.97	36.1	6.09	4
32	2.98	32.8	27.1	8
48	2.97	37.1	50.68	12
64	2.78	42.7	121.68	12

n_{ele}	Structure	Fluid	ALE	Total
16	2,592	9,612	7,209	19,413
32	14,688	71,444	53,583	139,715
48	44,352	189,916	142,437	376,705
64	96,960	540,956	405,171	1,043,087

Monolithic System of Equations

Linear System of Equations

- We exemplarily choose the structure field as master field \rightarrow structure-handled interface motion

$$\begin{bmatrix} \mathcal{S}_{II} & \mathcal{S}_{IF} \\ \mathcal{S}_{GI} & \mathcal{S}_{FF} \end{bmatrix} \begin{bmatrix} \mathcal{F}_{II} & \mathcal{F}_{IF} \\ \mathcal{F}_{GI} & \mathcal{F}_{FF} \end{bmatrix} \begin{bmatrix} \mathcal{F}_{II}^G & \mathcal{F}_{IF}^G \\ \mathcal{F}_{GI}^G & \mathcal{F}_{FF}^G \end{bmatrix} \begin{bmatrix} \mathcal{A}_{II} & \mathcal{A}_{IF} \end{bmatrix} \begin{bmatrix} -(1-a)\mathcal{M}^T \\ (1-b)\mathcal{D}^T \end{bmatrix} = \begin{bmatrix} \Delta d_{\Gamma,p}^S \\ \Delta d_{\Gamma,p}^G \end{bmatrix}$$

$$-\mathcal{M} \quad \tau\mathcal{D} \quad \mathcal{M} \quad -\mathcal{D} \quad \begin{bmatrix} \Delta d_{\Gamma,p}^S \\ \Delta d_{\Gamma,p}^G \end{bmatrix} = \begin{bmatrix} \mathbf{r}_{\Gamma}^S \\ \mathbf{r}_{\Gamma}^G \end{bmatrix} + \begin{bmatrix} 0 \\ -a\mathcal{M}^T \lambda^n \end{bmatrix} + b\mathcal{D}^T \lambda^n + \delta_{i0} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \Delta t \mathcal{D} u_{\Gamma}^{F,n} - \mathcal{M} \Delta d_{\Gamma,p}^S$$

Condensation of Lagrange Multipliers

- Use balance of linear momentum of slave interface DOFs for condensation
- Dual Mortar method leads to diagonal form of Mortar matrix \mathcal{D}
- Computationally cheap condensation of Lagrange multipliers and slave interface DOFs

Adaptive Time Stepping: Numerical Example

- Thin-walled spherical structure with fluid loading
- Prescribed inflow velocity at top

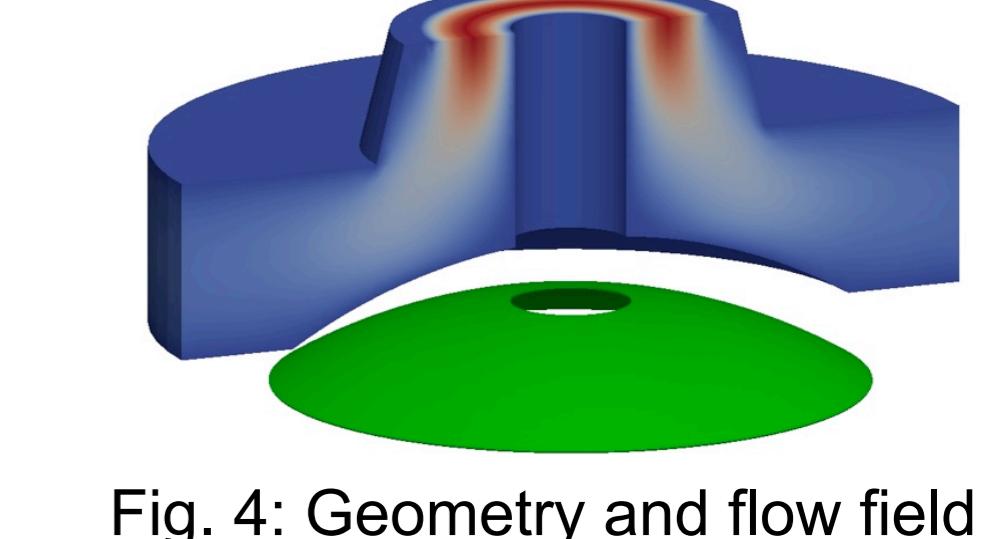
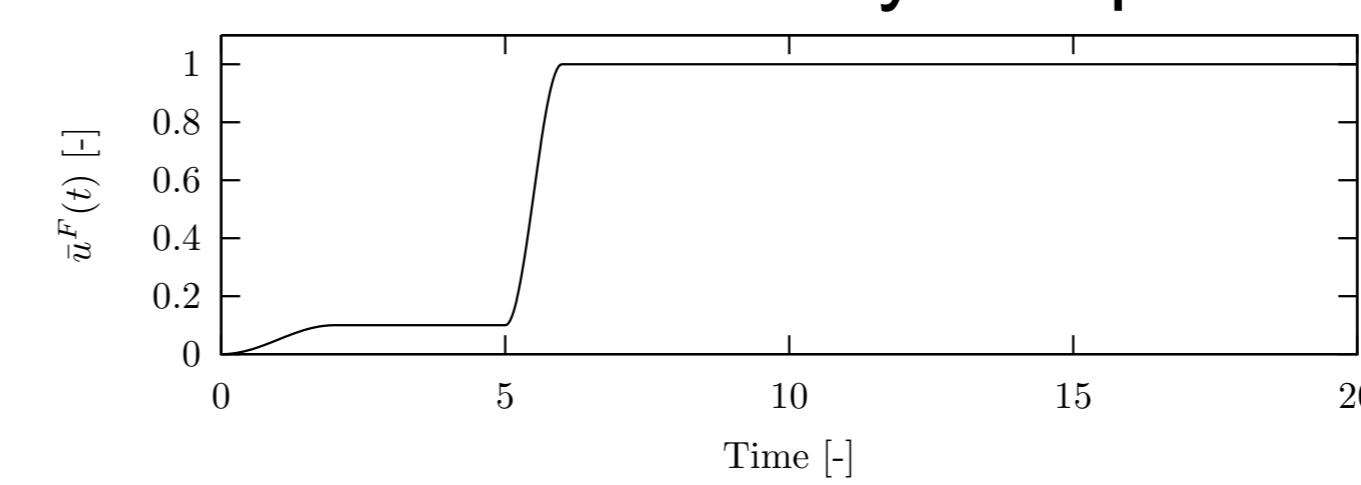


Fig. 5: Solution at end time after snap-through of structure

Main Results

- saving ca. 96% of number of computed time steps
- guaranteed level of accuracy

Nonlinear GMRES with AMG-FAS Preconditioning

- FAS: Full Approximation Scheme

- Variational residual evaluation

$$F_c = R_c^0 F_0 (P_c^c x_c)$$

- Motivation

- Timings: residual evaluation vs. linear solve
- residual evaluation scales perfectly for fine grained parallelization

- Idea

- nonlinear FSI-coupling on coarse levels using FSI-AMG hierarchy
- acceleration by outer nonlinear Krylov-type solver [5]

- Multigrid library: Trilinos/MueLu [6]

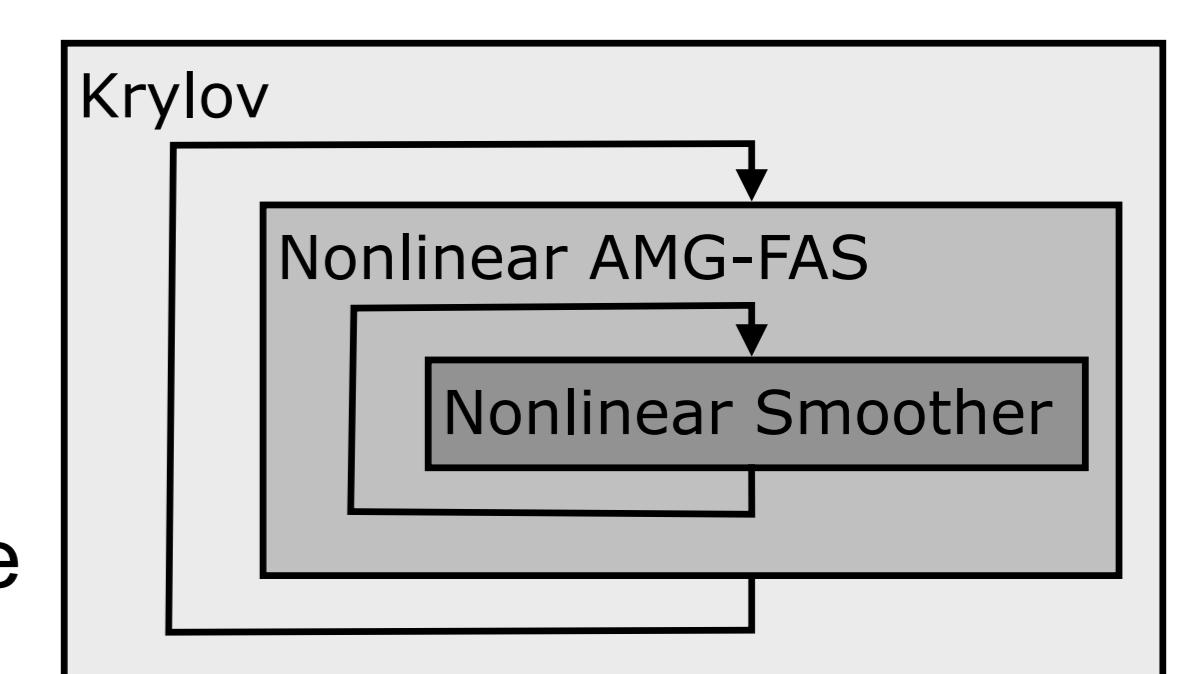


Fig. 8: Sketch of algorithm

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- [2] Klöppel T, Popp A, Kötter U, Wall WA: Fluid-structure interaction for non-conforming interfaces based on a dual mortar formulation, Comput. Methods Appl. Mech. Engrg., 200(45-46):3111-3126, 2011
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- [6] Prokopenko A, Hu JJ, Wiesner TA, Siebert CM, Tuminaro RS: MueLu User's Guide 1.0, Techn. Report SAND2014-18874, Sandia National Laboratories, 2014