

# A temporal consistent monolithic approach to fluid-structure interaction enabling single field predictors



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## Introduction

### Motivation and goals

- Possibility to choose time integration scheme in structure and fluid field differently and tailored to the needs of the respective field
- Interpolation of interface traction in presence of different temporal discretizations in structure and fluid field in order to avoid possible stability problems [1]
- Enable field specific predictors in order to reduce computational costs

## Problem Definition

### Domain of interest

- Structural domain  $\Omega^S$  (governed by elastodynamics)
- Fluid-ALE domain  $\Omega^F$  (governed by Navier-Stokes equations)
- Fluid-structure interface  $\Gamma_{FSI}$

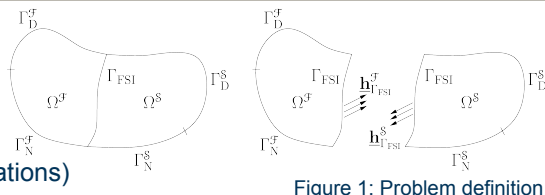


Figure 1: Problem definition

### Coupling conditions at fluid-structure interface

- Weak enforcement of kinematic coupling condition by Lagrange multiplier field  $(\delta \lambda, \mathbf{d}_{\Gamma_{FSI}}^S - \mathbf{d}_{\Gamma_{FSI}}^F)_{\Gamma_{FSI}} = 0$  in  $\Gamma_{FSI} \times (0, T)$
- Identify Lagrange multiplier field as interface traction  $\lambda = \mathbf{h}_{\Gamma_{FSI}}^S = -\mathbf{h}_{\Gamma_{FSI}}^F$

## Discretization

### Spatial discretization of structure and fluid field

- Mixed/hybrid finite elements for structure field
- Stabilized finite elements for fluid field
- Distinguish between interface DOFs (subscript  $\Gamma$ ) and interior DOFs (subscript  $I$ )

### Spatial discretization of Lagrange multiplier field

- Dual Mortar method for Lagrange multiplier field [2]
- Distinguish between *master* and *slave* side due to Mortar method

### Temporal discretization

- Temporal discretization with *fully implicit, single-step, single-stage* time integration schemes with dynamic equilibrium at generalized mid-point  $t^m$
- Different time integration schemes in structure and fluid field  $\rightarrow t^{S,m} \neq t^{F,m}$
- Single field predictors might result in a gap  $\Delta \mathbf{d}_{\Gamma,p}^S$  at the interface that has to be accounted for in the discrete kinematic coupling conditions.

### Discrete coupling conditions

- Kinematic continuity (accounting for possible predictors)

$$\mathbf{c}_{SF} \Delta \mathbf{d}_{\Gamma,i+1}^{S,n+1} + \delta_{i0} \mathbf{c}_{SF} \Delta \mathbf{d}_{\Gamma,p}^S = \tau \mathbf{c}_{FS} \Delta \mathbf{u}_{\Gamma,i+1}^{F,n+1} + \delta_{i0} \Delta t \mathbf{c}_{FS} \mathbf{u}_{\Gamma}^{F,n}$$

- Dynamic coupling conditions have to respect possible different time integrators in structure and fluid field. Hence, the Neumann-like interface traction has to be incorporated into the balances of linear momentum at the respective generalized mid-point  $t^{S,m}$  or  $t^{F,m}$  by interpolation (Fig. 2):

$$\mathbf{r}_{\lambda,i}^{S,m} = -\mathbf{c}_{SF}^T (a \lambda^n + (1-a) \lambda_i^{n+1})$$

$$\mathbf{r}_{\lambda,i}^{F,m} = \mathbf{c}_{FS}^T (b \lambda^n + (1-b) \lambda_i^{n+1})$$

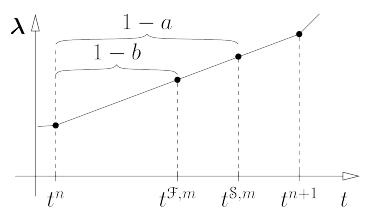


Figure 2: Temporal interpolation

### Nonlinear FSI residual

$$\mathbf{r}^{FSI} = \begin{bmatrix} \mathbf{r}_{\lambda,\Gamma}^S \\ \mathbf{r}_{\lambda,\Gamma}^F \\ \mathbf{r}_{\lambda,\Gamma}^F \\ \mathbf{r}_{\lambda,\Gamma}^S \\ \mathbf{r}^{coupl} \end{bmatrix} + \begin{bmatrix} \mathbf{0} \\ \mathbf{r}_{\lambda,\Gamma}^S \\ \mathbf{0} \\ \mathbf{r}_{\lambda,\Gamma}^F \\ \mathbf{0} \end{bmatrix} = \mathbf{0}$$

### Linearization for Newton-Krylov solver

- Linearization with respect to unknown Lagrange multipliers

$$\frac{\partial \mathbf{r}_{\lambda,i}^{S,m}}{\partial \lambda_i^{n+1}} = -(1-a) \mathbf{c}_{SF}, \quad \frac{\partial \mathbf{r}_{\lambda,i}^{F,m}}{\partial \lambda_i^{n+1}} = (1-b) \mathbf{c}_{FS}$$

- Monolithic system of linearized equations

$$\begin{bmatrix} \frac{\partial \mathbf{r}_{\mathbf{d}}^S}{\partial \mathbf{x}^S} & \mathbf{0} & \frac{\partial \mathbf{r}_{\lambda}^S}{\partial \lambda} \\ \mathbf{0} & \frac{\partial \mathbf{r}_{\mathbf{u}}^F}{\partial \mathbf{x}^F} & \frac{\partial \mathbf{r}_{\lambda}^F}{\partial \lambda} \\ \frac{\partial \mathbf{r}^{coupl}}{\partial \mathbf{d}_F^S} & \frac{\partial \mathbf{r}^{coupl}}{\partial \mathbf{u}_F^F} & \mathbf{0} \end{bmatrix}^{n+1} \begin{bmatrix} \Delta \mathbf{x}^S \\ \Delta \mathbf{x}^F \\ \Delta \lambda \end{bmatrix}_{i+1} = - \begin{bmatrix} \mathbf{r}^S \\ \mathbf{r}^F \\ \mathbf{r}^{coupl} \end{bmatrix}_i$$

## Monolithic System of Equations

### Linear System of Equations

- We exemplarily choose the structure field as master field  $\rightarrow$  structure-governed interface motion  $\rightarrow$  Mortar coupling operators:  $\mathbf{c}_{SF} = \mathbf{M}$ ,  $\mathbf{c}_{FS} = \mathbf{D}$

$$\begin{bmatrix} \mathbf{S}_{II} & \mathbf{S}_{IF} \\ \mathbf{S}_{FI} & \mathbf{S}_{FF} \\ \mathbf{F}_{II} & \mathbf{F}_{IF} & \mathbf{F}_{II}^S & \mathbf{F}_{IF}^S \\ \mathbf{F}_{FI} & \mathbf{F}_{FF} & \mathbf{F}_{FI}^S & \mathbf{F}_{FF}^S \\ \mathbf{A}_{II} & \mathbf{A}_{IF} \\ \mathbf{M} & \tau \mathbf{D} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \Delta \mathbf{d}_{\Gamma}^S \\ \Delta \mathbf{d}_{\Gamma}^F \\ \Delta \mathbf{u}_{\Gamma}^S \\ \Delta \mathbf{u}_{\Gamma}^F \\ \Delta \mathbf{d}_{\Gamma}^S \\ \Delta \mathbf{d}_{\Gamma}^F \\ \lambda \end{bmatrix}_{i+1} = \begin{bmatrix} \mathbf{0} \\ \mathbf{0} \\ \mathbf{0} \\ \mathbf{0} \\ \mathbf{0} \\ \mathbf{0} \\ \Delta t \mathbf{D} \mathbf{u}_{\Gamma}^{F,n} - \mathbf{M} \Delta \mathbf{d}_{\Gamma,p}^S \\ \mathbf{M} \Delta \mathbf{d}_{\Gamma,p}^S \end{bmatrix}_{i+1}$$

### Condensation of Lagrange multipliers

- Use balance of linear momentum of slave interface DOFs for condensation
- Dual Mortar method leads to diagonal form of Mortar matrix  $\mathbf{D} \rightarrow$  Computationally cheap condensation of Lagrange multipliers and slave interface DOFs

## Numerical Examples

### Pseudo 1D FSI example with analytical solution

- Temporal convergence study with different time integrators in structure and fluid field (Fig. 4)
- Overall order of accuracy depends on single field accuracy  $\rightarrow$  second order accuracy only if all time integrators are second order accurate

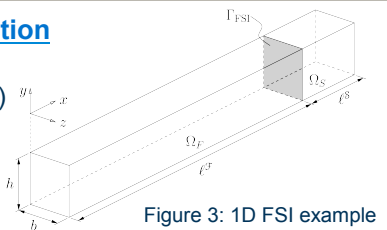


Figure 3: 1D FSI example

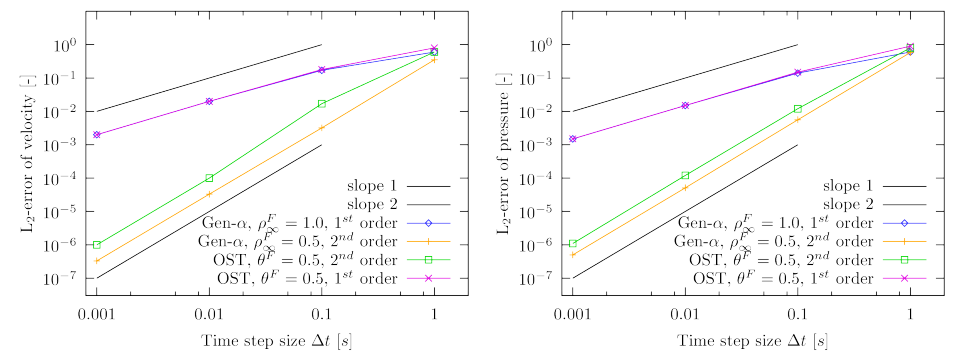


Figure 4: Temporal convergence of L2-error in velocity and pressure field

### 2D leaky driven cavity with flexible bottom

- Number of linear iterations reflects computational costs
- Reference solution without predictor (ConstDis)
- Reduction of number of linear iterations by 10% on average by employing simple predictors in structure field like constant velocity assumption (ConstVel) or constant acceleration assumption (ConstAcc) (see Fig. 5)

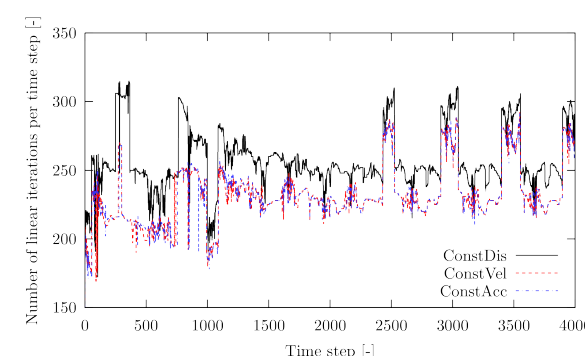


Figure 5: Saving of linear iterations as measure of computational costs

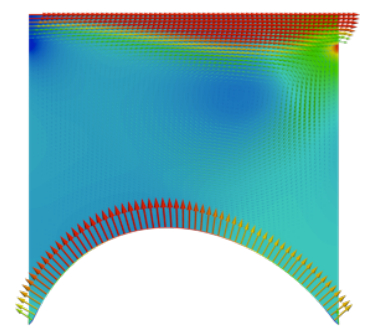


Figure 6: Velocity, pressure and Lagrange multiplier field

## References

- [1] Joosten MM, Dettmer WG, Peric D. On the temporal stability and accuracy of coupled problems with reference to fluid-structure interaction. *Int. J. Numer. Meth. Fluids*, 64 (10-12): 1363-1378, 2010.
- [2] Klöppel T, Popp A, Küttler U, Wall WA. Fluid-structure interaction for non-conforming interfaces based on a dual mortar formulation. *Comput. Methods Appl. Mech. Engrg.*, 200 (45-46): 3111-3126, 2011.
- [3] Mayr M, Klöppel T, Wall WA, Gee MW. A temporal consistent monolithic fluid-structure interaction approach enabling single field predictors, *in preparation*.