

# Site-Selective Enhancement of Superconducting Nanowire Single-Photon Detectors via Local Helium Ion Irradiation

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Achieving homogeneous performance metrics between nominally identical pixels is challenging for the operation of arrays of superconducting nanowire single-photon detectors (SNSPDs). Here, local helium ion irradiation is utilized to post-process and tune single-photon detection efficiency, switching current, and critical temperature of individual devices on the same chip. For 12 nm thick highly absorptive SNSPDs, which are barely sensitive to single photons with a wavelength of 780 nm prior to He ion irradiation, an increase of the system detection efficiency from  $<0.05\%$  to  $(55.3 \pm 1.1)\%$  is observed following irradiation. Moreover, the internal detection efficiency saturates at a temperature of 4.5 K after irradiation with  $1800 \text{ ions nm}^{-2}$ . Compared to 8 nm SNSPDs of similar detection efficiency, a doubling of the switching current (to  $20 \mu\text{A}$ ) is observed for irradiated 10 nm thick detectors, increasing the amplitude of detection voltage pulses. Investigations of the scaling of superconducting thin film properties with irradiation up to a fluence of  $2600 \text{ ions nm}^{-2}$  revealed an increase of sheet resistance and a decrease of critical temperature towards high fluences. A physical model accounting for defect generation and sputtering during helium ion irradiation is presented and shows good qualitative agreement with experiments.

superior performance metrics, consisting of high detection efficiency also at long wavelengths,<sup>[13,14]</sup> low dark count rate,<sup>[15]</sup> and low timing jitter<sup>[16]</sup> make them ideally suited for demanding applications such as quantum key distribution,<sup>[2–4]</sup> quantum computing,<sup>[17]</sup> or deep space optical communication.<sup>[7]</sup> Moreover, their waveguide-integrated form is a key component for photonic integrated circuits.<sup>[18–22]</sup>

Since recently, SNSPDs also find application in fields such as astronomy,<sup>[23]</sup> dark matter detection,<sup>[24]</sup> and particle detection.<sup>[25,26]</sup> However, these applications typically require large detector arrays or even an SNSPD camera, which to date turns out to be challenging due to the necessary readout and homogeneity within an ensemble of the order of hundreds to thousands of detectors. Recently, row–column multiplexing of a 1024-pixel array,<sup>[27]</sup> and a promising readout architecture based on thermal coupling and time-of-flight measurements<sup>[28]</sup> were demonstrated. For such pixel arrays, typically amorphous

materials such as MoSi and WSi are used, although SNSPDs based on polycrystalline materials like NbN and NbTiN exhibit higher critical temperatures, larger critical currents, and lower timing jitter. Compared to polycrystalline materials and their spatial inhomogeneities of the superconducting energy gap,<sup>[29–32]</sup> amorphous films attain better homogeneity and the associated

## 1. Introduction

Superconducting nanowire single-photon detectors (SNSPDs)<sup>[1]</sup> play a significant role in quantum technologies<sup>[2–9]</sup> and a wide range of applications requiring general faint light detection.<sup>[10,11]</sup> Compared to single-photon avalanche diodes (SPADs),<sup>[12]</sup> their

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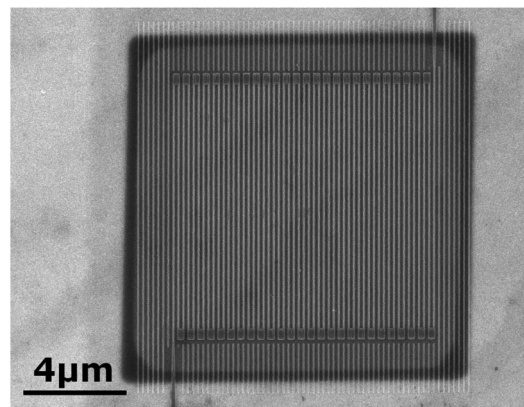
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higher yield of similarly performing detectors.<sup>[33–37]</sup> To enable the use of NbN for large pixel arrays, atomic layer deposition and molecular-beam epitaxy of highly homogeneous films have been investigated recently as alternatives to the common deposition of polycrystalline NbN and NbTiN films grown using reactive magnetron sputtering.<sup>[38–41]</sup> In addition to methods for obtaining better homogeneity during film deposition, a method to tune detector metrics of individual devices after fabrication would also be highly advantageous. Inspired by the recent work of Zhang et al.,<sup>[42]</sup> which sparked interest in irradiating SNSPDs with helium (He) ions,<sup>[43–45]</sup> we use a He ion microscope as a post-processing tool to tune detector metrics of individual NbTiN devices fabricated on the same chip. At the same time, we investigate how SNSPD properties such as detection efficiency and switching current depend on the He ion fluence. In addition to detector metrics, we explore the scaling of NbTiN thin film parameters such as sheet resistance and critical temperature with increasing irradiation.

## 2. Experimental Section

To study the influence of He ion irradiation on the native transport properties of NbTiN thin films and the performance of SNSPDs, NbTiN films with thicknesses of 8, 10, and 12 nm were deposited using DC reactive magnetron sputtering onto Si substrates with a 130 nm thick thermally grown SiO<sub>2</sub> layer. The NbTiN thickness was controlled by measuring the sputtering rate and adjusting the sputtering time correspondingly. Subsequently, the NbTiN films were patterned into cloverleaf structures and SNSPDs using electron beam lithography and reactive ion etching, followed by optical lithography and gold evaporation for contact pad fabrication.<sup>[46]</sup> The detector design consisted of a 100 nm wide wire in a meander form with a fill factor of 50%, and a total active area of 10 μm × 10 μm. The cloverleaf structures were fabricated in order to perform magneto-transport measurements in van-der-Pauw geometry<sup>[47,48]</sup> with an active area of 10 μm × 10 μm and to correlate the results of macroscopic transport with the He ion fluence dependent performance metrics of the corresponding SNSPDs. To ensure the best comparability, cloverleaves (CLs) and SNSPDs were fabricated on the same chip. For this study, they were subsequently irradiated with a He ion microscope (Zeiss Orion Nanofab) with He ion fluences ranging from 0 to 2600 ions nm<sup>-2</sup>. An acceleration voltage of 30 kV, an aperture of 10 and 20 μm, and beam currents between 0.3 and 114 pA were chosen, with the largest aperture and beam current used for the largest He ion fluences to obtain irradiation times of less than 30 min per device also for the largest fluences. Despite the sub-nanometer resolution of the He ion microscope, which makes it also attractive as a patterning tool for SNSPD fabrication,<sup>[49–51]</sup> focusing the He ion beam to smallest beam sizes was not necessary in this work since an area slightly larger than the active area of the SNSPDs and CLs was homogeneously irradiated as shown in **Figure 1** and the inset of **Figure 8**. The irradiation induced film surface roughness was measured with an atomic force microscope (Bruker Dimension Icon) in peak force tapping mode.

The magneto-transport measurements were performed by cooling the samples to 4.2 K before allowing them to slowly heat



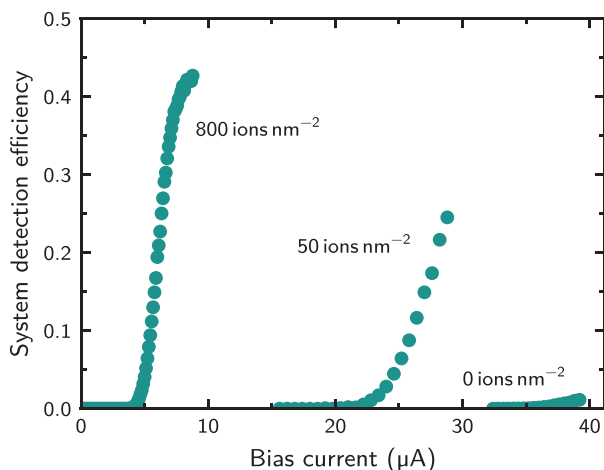
**Figure 1.** Scanning electron microscope image of an SNSPD after He ion irradiation. The irradiated area is visible as the dark shaded square region and was chosen to be slightly larger than the SNSPD to ensure homogeneous irradiation of the detector.

up to 20 K in external magnetic fields between  $-0.1$  and  $1$  T, applied perpendicular to the sample plane. From these measurements, the sheet resistance of the superconducting thin film at 20 K and room temperature, the critical temperature of the superconducting thin film, and the Bogoliubov quasiparticle diffusivity were extracted. Also, by measuring the CLs in Hall geometry and performing magnetic field sweeps, followed by a linear fit of the Hall voltage, the Hall coefficient and electron density of the NbTiN films were determined.<sup>[52]</sup>

Switching current  $I_{sw}$  and system detection efficiency (SDE) of the SNSPDs were measured using a cryogenic probe station (Janis) at 4.5 K. To determine the switching current, the voltage  $U_{app}$  applied across the SNSPD and a 50 kΩ resistor connected in series was ramped up, while measuring the current  $I_{meas}$ . The switching current was then defined as the current at which the criterion  $U_{app}/I_{meas} > 50.5$  kΩ was fulfilled for the first time. To calculate the SDE, the dark count rate (DCR) was determined before measuring the count rate (CR) by homogeneous illumination of the SNSPD with an attenuated and collimated 780 nm continuous wave diode laser with a spot size of  $(1.1 \pm 0.1)$  mm (full width at half maximum of the intensity profile) and polarization parallel to the nanowire. The SDE is then defined as  $SDE = \frac{CR - DCR}{PR}$  with the photon rate PR incident on the cryogenic probe station.

## 3. Results and Discussion

In this section, we present the dependence of NbTiN thin film properties and detector metrics on He ion irradiation for film thicknesses of 8, 10, and 12 nm. Provided that the SNSPDs are sensitive to single photons, using larger thicknesses for SNSPDs generally results in stronger optical absorption<sup>[53,54]</sup> and therefore enhances their overall system detection efficiency (SDE). Moreover, we aim for a better understanding of how He ion irradiation modifies the transport properties of the NbTiN film and focus on establishing structure–property relationships that link detector thickness, He ion fluence, and detector performance.

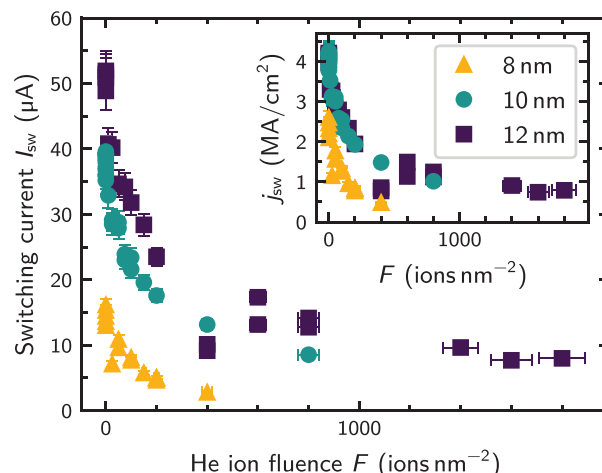


**Figure 2.** System detection efficiency versus bias current of the same 10 nm thick detector for three different He ion fluences. The relative uncertainties of He ion fluence, SDE, and bias current are 5%, 2%, and less than 1%, respectively (error bars not shown for clarity). The measurements were performed at a temperature of 4.5 K and using photons with a wavelength of 780 nm. With increasing fluence the efficiency rises up to 43% and shows the beginning of saturating internal detection efficiency, while the switching current decreases. The largest change in SDE and  $I_{sw}$  is induced by the first He ions that hit the detector.

### 3.1. Performance of He Ion Irradiated SNSPDs

**Figure 2** shows the increase in SDE and the simultaneous decrease of switching current of a representative 10 nm thick device measured before irradiation and after fluences of 50 and 800 ions  $\text{nm}^{-2}$ . Irradiating the detector with 50 ions  $\text{nm}^{-2}$  already results in an increase in SDE from <2% to 25%. At a fluence of 800 ions  $\text{nm}^{-2}$  the detector shows the beginning of saturating SDE at 43%, close to the maximum absorption of 53.1% in the detector as determined by finite-difference time-domain (FDTD) simulations (Appendix A). Simultaneously, a decrease in switching current  $I_{sw}$ , which is defined as the maximum current the detector can sustain before switching to the normal conducting state, is apparent and ranges from 39.2 to 28.8 and 8.6  $\mu\text{A}$  after irradiation.

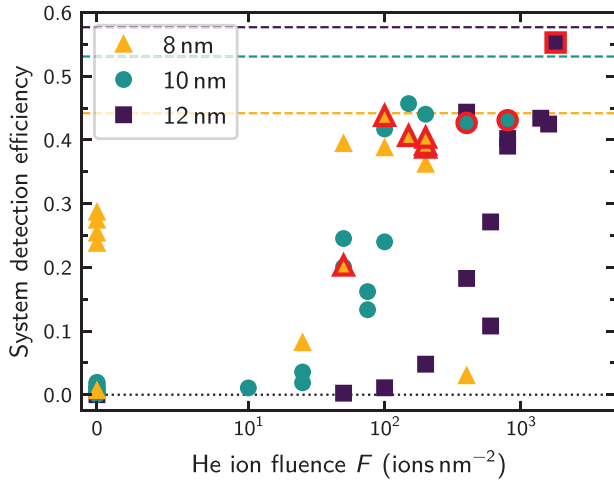
To study the scaling of the switching current with He ion fluence, we irradiated multiple detectors that have thicknesses of 8, 10, and 12 nm using different He ion fluence values. **Figure 3** shows the resulting data, revealing a clear trend of decreasing  $I_{sw}$  with He ion fluence. As expected,  $I_{sw}$  is higher for thicker devices of the same fluence due to the larger cross-sectional area of thicker nanowires. We explain the scattering of measured switching currents of nominally identical detectors by constrictions that limit  $I_{sw}$  to a lower value than non-constricted devices have.<sup>[35]</sup> Such scatter is particularly visible by the large variation of currents of the non-irradiated devices and the small values of the two 12 nm detectors irradiated with 400 ions  $\text{nm}^{-2}$ . The inset of **Figure 3** shows the switching current density  $j_{sw}$  as calculated from  $I_{sw}$  and the cross sectional area of the wire, given by the width and the nominal wire thickness presented in Table A1. Furthermore, we accounted for an effective reduction of the nominal thickness due to surface sputtering during He ion irradiation as derived in Section 3.2 and for a native NbTiN oxide of 1.3 nm thickness.<sup>[55]</sup> The switching current density of our non-



**Figure 3.** Switching current versus He ion fluence for 8, 10, and 12 nm detector thickness, including statistical errors.  $I_{sw}$  decreases with the He ion fluence, showing the largest decrease for low fluences. A strong dependence of  $I_{sw}$  on the film thickness is apparent throughout the whole fluence range studied. The inset shows the switching current density  $j_{sw}$  as calculated from  $I_{sw}$  and the wire width and thickness, accounting for an effective thickness reduction due to surface sputtering during He ion irradiation as well as a 1.3 nm thick native NbTiN oxide. The large data point clusters at 0 ions  $\text{nm}^{-2}$  originate from measurements of a large subset of devices before irradiation.

irradiated NbTiN detectors is comparable to the data Korneeva et al.<sup>[56]</sup> present for 5.8 nm thick NbN devices. Moreover, we observe  $j_{sw}$  of the 8 nm film being smaller than for the 10 and 12 nm films. We note that for thin and narrow wires, the depairing current density<sup>[56,57]</sup> can limit the measurable switching current density and reveals a dependence on the film thickness.<sup>[58,59]</sup> Thus, an increased depairing current density for the thicker devices also likely contributes to their higher  $I_{sw}$  and  $j_{sw}$ . Furthermore, the limiting critical current of our devices presumably occurs at the hairpin turns of the nanowires due to current crowding, especially at temperatures well below the critical temperature.<sup>[60–62]</sup>

Similar to  $I_{sw}$ , we investigated the scaling of SDE with the He ion fluence. As shown in **Figure 4**, we observe an increase of SDE with the He ion fluence for all detector thicknesses, despite the large scatter between data obtained from nominally identical SNSPDs. Most notably, the SDE for the 12 nm thick detectors increases from less than 0.05% for the non-irradiated case to 55.3% and just saturating detection efficiency for a fluence of 1800 ions  $\text{nm}^{-2}$ . As expected, the SDE increases with detector thickness due to the higher absorption. The dashed horizontal lines in **Figure 4** show the upper limit for the SDE, defined by the absorption of SNSPDs of the respective thicknesses that we obtained from FDTD simulations discussed in Appendix A. We note that one can further enhance the absorption and thus the SDE over a broad wavelength range by adding a metal mirror with an optical cavity underneath the SNSPD.<sup>[63]</sup> Recently, a similar approach for He ion irradiated detectors involving a narrow-band cavity, realized with a distributed Bragg reflector, has shown to push the absorption to over 90%.<sup>[43]</sup> The fact that the measured SDE of the highest irradiated 8 nm detector shown in **Figure 4** is less than 3% can be explained as follows: Due to the irradiation-induced reduction of the switching current (to 2.8  $\mu\text{A}$  for this

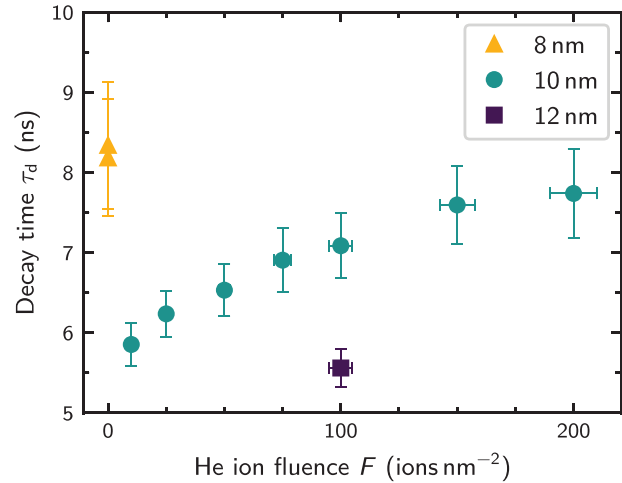


**Figure 4.** System detection efficiency versus He ion fluence for the three detector thicknesses studied in this work. Dashed lines indicate the absorption in the SNSPD simulated with FDTD; data points with saturating SDE are highlighted with a red frame. The relative uncertainties of SDE and He ion fluence are 2% and 5%, respectively (error bars not shown for clarity). Each of the data points stems from a different detector that was irradiated once with the given dose except for two 10 nm and two 12 nm detectors that were irradiated twice; for some SNSPDs we measured the SDE in addition also before irradiation. The measurements were performed at a wavelength of 780 nm. Despite the large scattering of data points that can be explained by the strong variation of the initial SDE between individual devices, one clearly sees that the SDE increases with He ion fluence and that the total maximum SDE is reached by the largest detector thickness.

detector), which is also the maximum applicable bias current, the maximum voltage pulse amplitude decreases as well. However, the trigger level of the counter used to measure the efficiency can only be reduced correspondingly as long as it is well above the electrical noise floor. This implies that once the pulse amplitude becomes comparable to the electrical noise floor, a substantial fraction of detection pulses will not be registered by the counter anymore. Depending on the readout electronics used and on their noise floor, this sets the limit for meaningful He ion fluences when irradiating SNSPDs. Surprisingly, one of the 12 nm/400 ions  $\text{nm}^{-2}$  detectors shown in Figure 4 exhibits a high SDE although  $I_{\text{sw}}$  was lower than expected for these two SNSPDs. This hints to a relatively homogeneous current density within the nanowire that allows biasing close to the depairing current density and thus achieving high SDE.

Another key metric for SNSPDs is their recovery time since it determines the detector's maximum count rate. It can be estimated from the time constant  $\tau_d$  of the exponential decay of a detection voltage pulse.<sup>[18,64]</sup> Figure 5 shows how the measured decay time increases with increasing He ion fluence and demonstrates that it is smaller for thicker detectors. These observations can be understood as follows: The decay time depends on the kinetic inductance  $L_k$  of the detector by  $\tau_d = L_k/R_{\text{load}}$  with a typical load resistance of  $R_{\text{load}} = 50 \Omega$  for the readout electronics.<sup>[64]</sup> At the same time,  $L_k$  of a thin and dirty superconducting film of length  $l$  and width  $w$  is given by

$$L_k = \frac{\hbar R_{\text{sheet}}}{\pi \Delta(0 \text{ K})} \frac{l}{w} \quad (1)$$



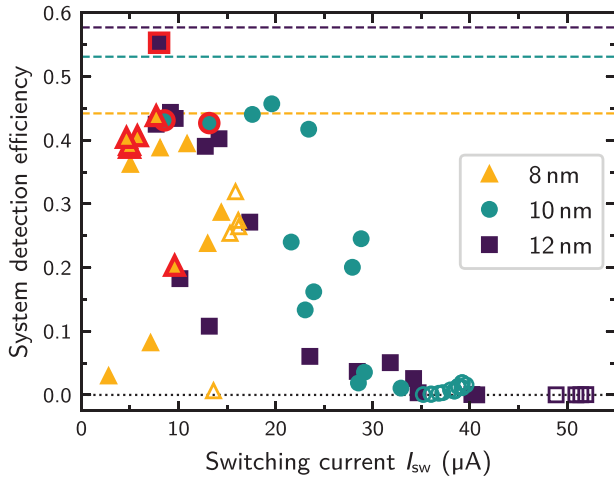
**Figure 5.** Decay time versus He ion fluence, including statistical errors.  $\tau_d$  increases with increasing fluence and decreasing thickness due to the resulting higher kinetic inductance of the detector.

as derived in Appendix B. Thus, for detectors of similar length and width, the kinetic inductance and the decay time are smaller for detectors that exhibit a smaller sheet resistance, for example due to the use of a thicker film or due to less irradiation with He ions. In this way, we conclude that the increase of decay time due to irradiation can be compensated to a certain extent by using thicker films.

For applications, simultaneously high SDE and  $I_{\text{sw}}$  are desired since a higher  $I_{\text{sw}}$  yields a higher detection pulse, which reduces not only the requirements for pulse detection with the readout electronics but also the timing jitter induced by electrical noise.<sup>[16,46]</sup> To compare these two performance metrics, Figure 6 shows the SDE against  $I_{\text{sw}}$  (open symbols representing the non-irradiated detectors, a red frame highlighting saturating SDE, and dashed lines indicating the simulated SDE upper limit). It is interesting to note how  $I_{\text{sw}}$  and SDE compare between the 8 nm and the 10 nm devices with an SDE between 39% and 46%: While providing a similar efficiency, the 10 nm devices offer twice as much switching current, 20  $\mu\text{A}$  instead of 10  $\mu\text{A}$ . This  $I_{\text{sw}}$  is also higher than that of the non-irradiated 8 nm detectors. Another comparison can be drawn between the 8 nm SNSPDs with saturating SDE close to 44% and the 12 nm SNSPD showing 55.3% SDE: at similar switching currents of about 8  $\mu\text{A}$ , the 12 nm SNSPD provides a substantially higher SDE. Furthermore, it is noteworthy that the shift of the data point clouds in this two-dimensional parameter space is not monotonic to higher  $I_{\text{sw}}$  with higher thickness (except for the non-irradiated devices). This could hint to the existence of an optimum thickness between 8 and 12 nm to reach simultaneous high SDE and  $I_{\text{sw}}$  via He ion irradiation: On the one hand, an increasing detector thickness results in an increase of switching current and absorption (see Appendix A). On the other hand, thicker films exhibit a lower sensitivity to actually detect an absorbed photon.

To conclude, by choosing a suitable detector thickness and He ion fluence, one can tune  $I_{\text{sw}}$  and SDE, even to better performance in both parameters simultaneously compared to non-irradiated detectors. Moreover, by individual irradiation of NbTiN





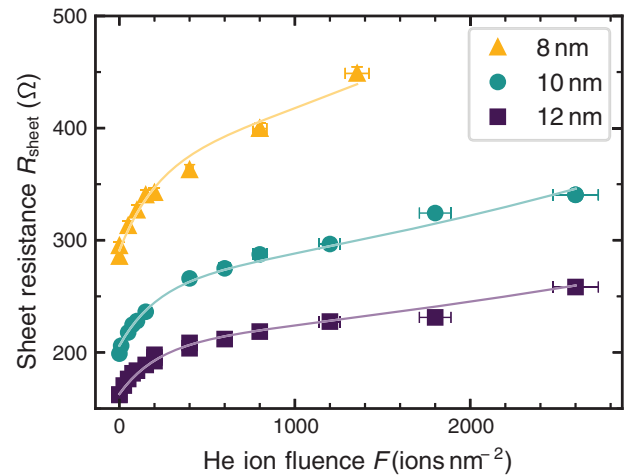
**Figure 6.** Maximum system detection efficiency versus switching current for the three detector thicknesses studied in this work. The simulated maximum SDE of each thickness is indicated by dashed lines, while saturating SDE is highlighted by symbols with a red frame; open symbols represent non-irradiated devices. The relative uncertainties of SDE and switching current are 2% and 6%, respectively (error bars not shown for clarity). Moreover, the SDE measurements were performed at a wavelength of 780 nm. Noteworthy are the data points at an SDE  $\approx$  45%, where the 10 nm SNSPDs provide a similar SDE like the 8 nm ones but offer the doubled switching current. Furthermore, for a similar  $I_{sw}$  of about 8  $\mu$ A, one 12 nm SNSPD shows up to 55.3% SDE, whereas the 8 nm ones provide only up to 43.8% SDE.

SNSPDs with a suitable He ion fluence, one can intentionally modify the performance of selected detectors or even mitigate differences between nominally identical devices.

### 3.2. Scaling of Thin Film Metrics with He Ion Fluence

To investigate how He ion irradiation impacts upon the bare NbTiN film metrics such as critical temperature  $T_c$ , sheet resistance  $R_{sheet}$ , and electron density  $n_e$ , we fabricated cloverleaf structures together with the detectors on the same sample to perform magneto-transport measurements in van-der-Pauw geometry. In **Figure 7** we present the dependence of the sheet resistance  $R_{sheet}$  on the He ion fluence. As expected,  $R_{sheet}$  is higher for thinner films and increases with increasing He ion fluence as the number of defects in the NbTiN film increases. Interestingly, the sheet resistance does not scale as  $R_{sheet} = \rho/d_0$  with the nominal film thickness  $d_0$  as expected if all samples had the same specific resistivity  $\rho$ . Even if one subtracts a 1.3 nm thick layer of oxidized NbTiN<sup>[55]</sup> from the nominal NbTiN thickness, the resulting resistivities of the non-irradiated films are still lower for the thicker films than for the 8 nm film (1.94, 1.73, and 1.73  $\mu\Omega$  m for the 8, 10, and 12 nm films, respectively). Although one might expect  $R_{sheet}$  to saturate at high fluences due to a saturating defect density in the film, we experimentally observe a continuous increase of  $R_{sheet}$  with He ion fluence. This could have its origin in noticeable surface sputtering<sup>[65]</sup> and intermixing<sup>[66]</sup> at the film/substrate interface by the impinging He ions and an associated reduction of the effective film thickness.

Based on these observations and taking the sheet resistance to be directly proportional to the defect density, we develop a simple



**Figure 7.** Sheet resistance versus He ion fluence for 8, 10, and 12 nm film thickness, including statistical errors. The sheet resistance increases with He ion fluence and decreasing film thickness. All three data sets are described by the fit function given by Equation (5) with the parameters of Table 1.

physical model. In our model, each ion that passes through the film can create a defect cluster of an average volume  $v_D$  with an efficiency  $\eta$ . Moreover, we consider the film volume  $V$  as divided into many volume elements  $v_i$  with the same size as the average defect cluster volume  $v_D$ , and defect clusters may only be created in volume elements that do not already contain a defect cluster. Those considerations imply that irradiating a film of volume  $V$ , thickness  $d$ , and area  $A$  using a He ion fluence  $\Delta F$  creates  $\Delta N_D$  new defect clusters according to

$$\Delta N_D = \left( \frac{V - N_D v_D}{V} \right) \left( \frac{d}{\sqrt[3]{v_D}} \right) \eta A \Delta F. \quad (2)$$

The first fraction represents the fraction of  $V$  that does not yet contain defect clusters, the second fraction represents the number of potential defect clusters that an impinging ion could create when passing the film along its thickness. Dividing this equation by the total volume  $V$  to obtain an expression for the defect cluster density  $n_D$  and taking the limit  $\Delta F \rightarrow 0$  yields

$$\frac{dn_D}{dF} = \frac{\eta}{\sqrt[3]{v_D}} (1 - v_D n_D(F)). \quad (3)$$

This differential equation has the solution

$$n_D(F) = \frac{1}{v_D} \left( 1 - (1 - n_{D,0} v_D) e^{-\eta \sqrt[3]{v_D} F} \right), \quad (4)$$

where  $n_{D,0}$  is the defect cluster density of the non-irradiated film. We relate the defect cluster density to the specific resistivity  $\rho$  via direct proportionality with a film-thickness dependent constant  $a_{d_0}$ . To arrive at a model for the sheet resistance, we further account for the previously mentioned surface sputtering due to He

**Table 1.** Fit parameters of the physical model according to Equation (5), describing the data in Figure 7. For each thickness, the fit function has its own fit parameter  $a_{d_0}/\nu_D$ , while the other parameters are independent of film thickness and therefore shared between the three fit functions.

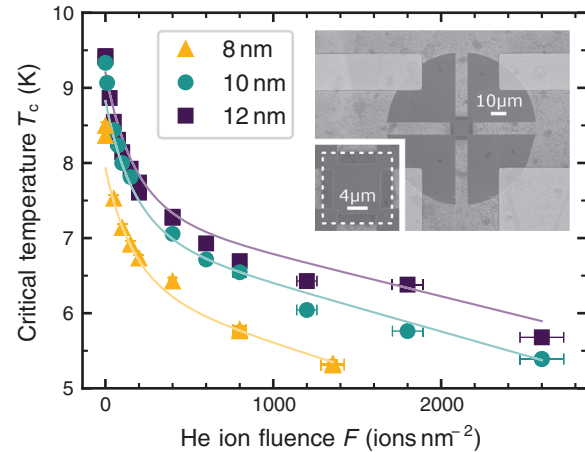
$d_0$ [nm]	$a_{d_0}/\nu_D$ [ $\Omega$ ]	$n_{D,0} \nu_D$	$\eta \nu_D^{2/3}$ [ $\text{nm}^2$ ]	$r_s$ [ $\text{nm}^3 \text{ion}^{-1}$ ]
8	$2957 \pm 36$			
10	$2618 \pm 36$	$0.79 \pm 0.01$	$(4.7 \pm 0.7) \times 10^{-3}$	$(9.4 \pm 6) \times 10^{-4}$
12	$2484 \pm 32$			

ion bombardment by including an effective reduction of the original film thickness  $d_0$  with a sputtering rate  $r_s$  and conclude

$$R_{\text{sheet}}(F) = \frac{1}{\nu_D} \left( 1 - (1 - n_{D,0} \nu_D) e^{-\eta \nu_D^{2/3} F} \right) \frac{a_{d_0}}{d_0 - r_s F}. \quad (5)$$

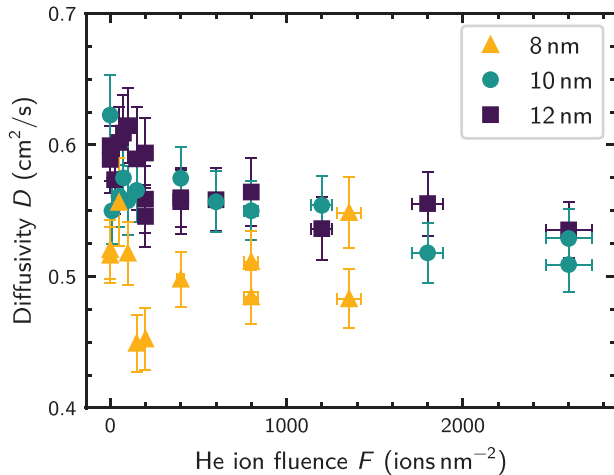
We fit this model to the experimental data and present the results of this fitting in Figure 7. Since the sputtering rate  $r_s$  and the factors  $n_{D,0} \nu_D$  and  $\eta \nu_D^{2/3}$  contain only thickness-independent quantities, we choose these factors as common fit parameters for all three thicknesses. In this way,  $a_{d_0}/\nu_D$  is the only individual fit parameter for each thickness, while the other three previously mentioned parameters are shared between all films. As such, we fit the three data sets with six parameters. **Table 1** lists the parameters that result in the fit functions shown in Figure 7. Considering the volume  $V$  as divided into many volume elements  $v_i$  with the same size as the average defect cluster volume  $\nu_D$ , the parameter  $n_{D,0} \nu_D$  can be qualitatively interpreted as the fraction of volume elements of the non-irradiated film that contains transport-related defective regions such as grain boundaries and scattering centers. We obtain  $n_{D,0} \nu_D = 0.79$ , indicating that the initial defect cluster density is high and/or the average volume of a defect cluster induced by a single He ion collision is on the order of the NbTiN grain size. A high defect density is not unexpected for a polycrystalline material such as NbTiN, and a defect cascade induced by a single He ion can extend over a volume similar to the NbTiN grain size (few nm) according to a study of He ion irradiation induced defect clusters in copper.<sup>[67]</sup> Within this model, the high value of 0.79 for  $n_{D,0} \nu_D$  means that most of the volume elements  $v_i$  are not available for modification by He ion irradiation. Furthermore, the quantity  $\eta \nu_D^{2/3}$  can be understood as the cross section determining the probability that an impinging He ion creates a defect cluster of volume  $\nu_D$ . Moreover, the sputtering rate of  $9.4 \times 10^{-4} \text{ nm}^3 \text{ ion}^{-1}$  implies that an irradiation by 1000 ions  $\text{nm}^{-2}$  leads to an effective reduction of the NbTiN film thickness by about 1 nm. Although Zhang et al.<sup>[42]</sup> did not observe a change in thickness after irradiating their NbN film with 500 ions  $\text{nm}^{-2}$ , our observation agrees well with the simulated and experimentally observed sputtering yield of typically 1 nm per 1000 ions  $\text{nm}^{-2}$  found in literature.<sup>[65,68]</sup>

**Figure 8** shows the dependence of the critical temperature  $T_c$  on the He ion fluence for 8, 10, and 12 nm thick films. Clearly,  $T_c$  decreases continuously by about 30% from the non-irradiated film to the film irradiated with 1200 ions  $\text{nm}^{-2}$ . Similarly to  $R_{\text{sheet}}$ , also  $T_c$  decreases most strongly for small He ion fluences. Interestingly, the measured values of  $T_c$  for the 10 and 12 nm films are very similar for low He ion fluences, although we would expect a lower  $T_c$  for the thinner film due to the suppression of



**Figure 8.** Critical temperature versus He ion fluence, including statistical errors.  $T_c$  decreases with He ion fluence, with the reduction in  $T_c$  at small fluences being the strongest. Surprisingly,  $T_c$  for the unirradiated 10 and 12 nm films are similar for small fluences, although  $T_c$  is typically higher for thicker films. The continuous functions we determined by fitting the  $T_c$  and  $R_{\text{sheet}}$  data with the universal scaling law introduced by Ivry et al.,<sup>[69]</sup>  $d_0 T_c = AR_{\text{sheet}}^{-B}$ , and subsequently using our physical model for  $R_{\text{sheet}}$ , given by Equation (5), as input to the universal scaling law. The inset shows an overview and a close-up view of the active area of an irradiated CL used for magneto-transport measurements (irradiated area highlighted by a white dashed square).

superconducting properties when transitioning from bulk to the nanoscale.<sup>[70–72]</sup> Furthermore, we fit our experimental data for  $T_c$  and  $R_{\text{sheet}}$  with the universal scaling law introduced by Ivry et al.,<sup>[69]</sup>  $d_0 T_c = AR_{\text{sheet}}^{-B}$ , which relates critical temperature, sheet resistance, and film thickness. Combining then the resulting fit function  $T_c(R_{\text{sheet}}, d_0)$  with our physical fit function for  $R_{\text{sheet}}$ , Equation (5), we obtain the fits shown in Figure 8. Appendix D contains details of the fitting procedure used for  $T_c$  and discusses the subtleties involved in interpreting the effective film thickness change due to He ion irradiation for  $R_{\text{sheet}}$  and  $T_c$ . A recent publication by Ruhtinas and Maasilta<sup>[73]</sup> contains a study of the critical temperature and the critical current density of comparably thick, 35 and 100 nm, NbTiN bridges, in which they suppressed superconductivity by He ion irradiation of a narrow line perpendicular to the bridge. Empirically, they observed a logarithmic dependence of  $T_c$  and an exponential dependence of  $j_{\text{sw}}$  on the He ion fluence  $F$ . As shown in Figure D3 in Appendix D, a fit of our data for the critical temperature with  $T_c(F) = -a \log(F + b) + c$  and fit parameters  $a$ ,  $b$ , and  $c$  for each of the three thicknesses describes our data even a bit better than the universal scaling law. However, using the universal scaling law, we need only the two fitting parameters  $A$  and  $B$  to describe all three data sets, while the empirical logarithmic fit function requires three fitting parameters for each thickness, a total of nine parameters for our three data sets. Moreover, our data for  $j_{\text{sw}}$  as shown in the inset of Figure 3 indicates that the switching current density does not follow the exponential dependence observed by Ruhtinas and Maasilta,<sup>[73]</sup> especially for the smaller He ion fluences. However, we note that compared to our work, Ruhtinas and Maasilta<sup>[73]</sup> studied the switching current density for higher fluences, ranging from  $2 \times 10^4$  to  $12 \times 10^4$  ions  $\text{nm}^{-2}$ . Furthermore, since the film thickness has



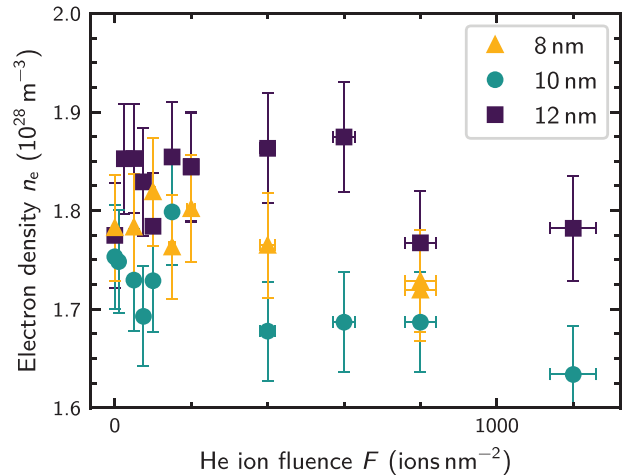
**Figure 9.** Quasiparticle diffusivity versus He ion fluence, including statistical errors.  $D$  is almost constant within the error bars, and averaging over all fluences reveals the thickness dependence of  $D$ . One might see a slight decrease of  $D$  with increasing fluence, which could be explained by the thickness reduction due to sputtering during He ion irradiation and the thickness dependence of  $D$ .

a strong influence on  $T_c$ , an interesting question is how the detectors'  $T_c$  compares between a thicker, higher irradiated SNSPD with a thinner, lower irradiated detector that both show a similar SDE. As elaborated in Appendix C, our data suggests that with the 10 nm detectors one can reach a similar SDE as with the 8 nm thick SNSPDs, while retaining a  $T_c$  of 8 K instead of 7.5 K. This is especially useful for applications with limited cooling powers.

Next, we investigate whether there is a systematic change of quasiparticle diffusivity  $D$  or electron density  $n_e$  with increasing He ion fluence. In addition to  $D$  and  $n_e$  being fundamental properties of the film, a reduction in diffusivity for example would result in a higher cut-off wavelength of photons detectable with the SNSPD and increase its sensitivity to single photons.<sup>[74,75]</sup> For this, we measured the temperature dependence of the upper critical magnetic field  $B_{c2}(T)$  by performing magneto-transport measurements while varying the temperature. From linear fits of  $B_{c2}(T)$  close to  $T_c$ , we extract the slope  $dB_{c2}/dT$  and calculate the diffusivity<sup>[53]</sup>

$$D = \frac{4k_B}{\pi e} \left[ \frac{dB_{c2}}{dT} \right]_{T \rightarrow T_c}^{-1} \quad (6)$$

Magnetic field sweeps were also performed with the film in the normal conducting state and at constant temperature, while measuring the Hall voltage  $V_H$ . Since  $V_H$  varies linearly with the applied magnetic field  $B$  and measurement current  $I$ , we determine the Hall coefficient  $R_H = V_H d_0 / (IB)$  using the slope of a linear fit of the  $V_H(B)$  data. From this, we estimate the electron density  $n_e$  according to  $R_H = -1/(n_e e)$  within the free electron model (see also refs. [52, 53, 76]). **Figures 9 and 10** show the quasiparticle diffusivity and the electron density as a function of the He ion fluence. Both are almost constant within the experimental error bars, although one might see a slight decrease of the diffusivity and the electron density with increasing He ion fluence. Since we usually observe decreasing electron density and diffusivity with



**Figure 10.** Electron density versus He ion fluence, including statistical errors. Despite fluctuations between measurements,  $n_e$  seems almost constant. One might see a slight decrease with increasing He ion fluence, which could be explained by the thickness dependence of  $n_e$  and the reduction of the effective film thickness during irradiation due to sputtering.

decreasing film thickness like Sidorova et al.,<sup>[52]</sup> this may be related to the observed effective thickness reduction of 0.94 nm per 1000 ions  $\text{nm}^{-2}$  due to sputtering during He ion irradiation.

#### 4. Conclusion and Outlook

In summary, we used a He ion microscope to locally tune the performance metrics of individual SNSPDs fabricated on the same chip. At the same time, our results demonstrated the possibilities of using thick (up to 12 nm) NbTiN films and He ion irradiation to enhance performance metrics such as system detection efficiency, switching current, decay time, and operating temperature compared to SNSPDs of smaller thicknesses. Thicker detectors exhibit higher optical absorption efficiency and shorter decay times as compared to similar SNSPDs fabricated from thinner films. However, due to the reduction of single-photon sensitivity with detector thickness, such SNSPDs typically offer only small detection efficiencies. Here, we have shown how He ion irradiation can boost the initially negligible SDE (<0.05%) of 12 nm thick SNSPDs by three orders of magnitude to 55.3% for a wavelength of 780 nm and at 4.5 K, resulting in an internal detection efficiency just within the saturated regime. This enables the use of thicker films and the associated advantages—at temperatures reachable with standard pulse-tube or Gifford–McMahon cryocoolers.<sup>[77]</sup> Furthermore, we found that by combining He ion irradiation and detectors fabricated from thicker films, one can enhance SDE and  $I_{sw}$  while reducing the decay time compared to non-irradiated smaller-thickness SNSPDs. While reduced decay times result in increased maximum count rates, higher  $I_{sw}$  and the associated higher detection voltage pulse imply a higher signal-to-noise ratio, which reduces the electrical noise induced timing jitter<sup>[16]</sup> and the necessary amplification of the electrical readout circuit.

Using a He ion microscope to irradiate individual detectors and cloverleaf structures on the same chip with different fluences allowed us to precisely study SNSPD and film properties

over He ion fluences ranging from 0 to 2600 ions nm<sup>-2</sup>, avoiding any errors that could arise from the high sensitivity of device properties on the exact sputtering or the subsequent fabrication process. We found that the increase of sheet resistance with the He ion fluence can be well described by a simple physical model that includes defect generation in the NbTiN film and an effective reduction of thickness due to sputtering during He ion bombardment. Moreover, the decrease of critical temperature with the He ion fluence can be described by combining our physical model for  $R_{\text{sheet}}$  with the universal scaling law from Ivry et al.,<sup>[69]</sup> which relates critical temperature, film thickness, and sheet resistance. At the same time, the quasiparticle diffusivity and electron density stay almost constant for the He ion fluences studied in this work. These magneto-transport measurements also show that irradiation of SNSPDs with He ions continuously changes their properties—although one can employ irradiation to enhance the SNSPD performance, excessive He ion irradiation ultimately leads to a vanishing, non-detectable signal when a photon is absorbed, rendering the SNSPD inoperative. These findings could be particularly interesting for applications where SNSPDs are exposed to radiation and high-energy particles.<sup>[25]</sup>

Besides the general enhancement of performance metrics of NbTiN SNSPDs by using thicker films combined with He ion irradiation, one can use targeted irradiation of individual devices with a He ion microscope for example in large SNSPD arrays to mitigate inhomogeneities of detector performance between pixels (or even dark pixels). This would be challenging without a post-processing technique such as site-selective He ion irradiation. Furthermore, targeted He ion irradiation enables the optimization of detectors for different performance metrics on the same chip, also after fabrication.

## Appendix A: Simulation of Optical Absorption in SNSPDs

The optical absorption in a detector provides an upper limit for its SDE. To determine the absorption for the detectors fabricated in this work, we performed finite-difference time domain (FDTD) simulations (Ansys Lumerical). Input parameters for these simulations are the width and thickness of the nanowire and the optical constants of the superconducting film that provides the basis for the detector. We controlled the thickness of the films by measuring the sputter deposition rate and selecting the deposition time accordingly. The optical constants of the thin films were measured with a variable angle spectroscopic ellipsometer (M-2000, J.A. Woollam Co.) and, as shown in **Table A1**, we observed an increase of the extinction coefficient with film thickness. Consequently, also for a thicker detector, the absorption does not only increase due to its larger

**Table A1.** Simulation parameters and results for the absorption in the 8, 10, and 12 nm thick detectors of this work.  $d_0$  is the nominal thickness of the detector, while  $w$  represents its mean wire width.  $n$  and  $k$  are refractive index and extinction coefficient of the underlying thin films, respectively. The absorption fraction  $\alpha$  denotes the percentage of light that is absorbed in the detector, obtained from FDTD simulations.

$d_0$ [nm]	$w$ [nm]	$n$	$k$	$\alpha$ [%]
8	92.6 ± 4.0	2.47	3.18	44.2
10	107.3 ± 1.9	2.48	3.33	53.1
12	115.3 ± 3.4	2.48	3.54	57.7

thickness but also due to the higher extinction coefficient of the thicker film. After detector fabrication, we evaluated the width of 22 representative detectors (Genesys ProSEM) and determined their mean wire width as listed in Table A1. Moreover, for the simulations we chose a plane-wave source with its polarization parallel to the nanowire, in line with the experiment. Table A1 shows the simulation input parameters and results for the optical absorption of the detectors of this work. The design of all detectors consists of 100 nm wide wires and a fill factor of 50% as described in Section 2. The measured width of the fabricated detectors deviates from this nominal value due to slight under-/overexposure during electron-beam lithography. This, however, does not change the reasoning within this work: For the same pitch, increased wire width (increased fill factor) or increased thickness both increase optical absorption and switching current, while reducing the detector's sensitivity to single photons.

## Appendix B: Kinetic Inductance of Thin and Dirty Superconducting Films

The kinetic inductance  $L_k$  of a thin ( $d \ll \lambda_{\text{eff}}$ ) and dirty ( $\ell \ll \xi_0$ ) superconducting film of length  $l$ , width  $w$ , and thickness  $d$  is given by

$$L_k = \mu_0 \lambda_{\text{eff,tf}} \frac{l}{w}, \quad (\text{B1})$$

with the effective magnetic penetration depth for thin films  $\lambda_{\text{eff,tf}} = \lambda_{\text{eff}}^2/d$  as introduced by Pearl,<sup>[78]</sup> where  $\lambda_{\text{eff}}$  is the effective magnetic penetration depth of a dirty bulk superconductor like NbTiN, given by

$$\lambda_{\text{eff}} = \lambda_L \sqrt{\frac{\xi_0}{\ell}} = \sqrt{\frac{\hbar \rho}{\pi \mu_0 \Delta(0 \text{ K})}}, \quad (\text{B2})$$

according to Bartolf [79, Equation (9.36)]. Here,  $\lambda_L$  is the London penetration depth,  $\xi_0$  the BCS coherence length,  $\ell$  the mean free path,  $\rho$  the specific resistivity of the superconducting film in the normal conducting state, and  $\Delta(0 \text{ K})$  the superconducting energy gap.<sup>[80,81]</sup> Hence, with the effective magnetic penetration depth one can express the kinetic inductance as

$$L_k = \mu_0 \frac{\lambda_{\text{eff}}^2}{d} \frac{l}{w} = \frac{\hbar R_{\text{sheet}}}{\pi \Delta(0 \text{ K})} \frac{l}{w}. \quad (\text{B3})$$

## Appendix C: Comparison of $T_c$ and SDE

The critical temperature  $T_c$  of SNSPDs is especially important for applications with limited cooling capabilities. In this section, we address the question how  $T_c$  compares between thicker, higher irradiated detectors and thinner, lower irradiated SNSPDs that both show a similar SDE. For this, we compare the detector's SDE with the thin-film  $T_c$  in **Figure C1**. The data suggests that with 44% the 10 nm detectors can actually reach an SDE comparable to the 8 nm SNSPDs, while retaining a  $T_c$  of 8 K instead of 7.5 K. This can be particularly useful for applications because a higher  $T_c$  reduces the requirements for the cooling system to operate the SNSPDs.

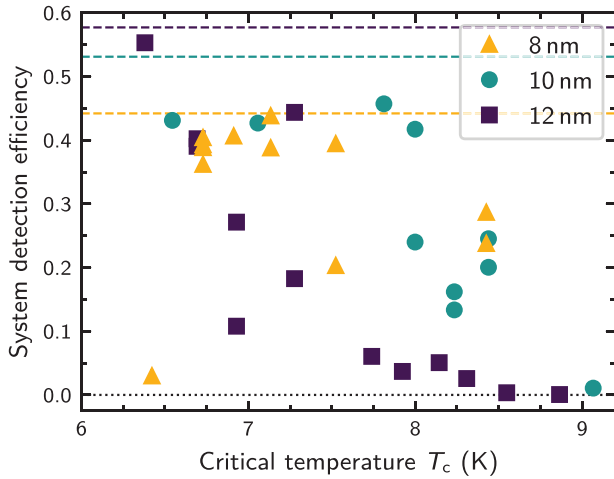
## Appendix D: Fitting of $T_c$ with Universal Scaling Law

To describe the data for the critical temperature in **Figure 8**, we use the universal scaling law, introduced by Ivry et al.,<sup>[69]</sup>

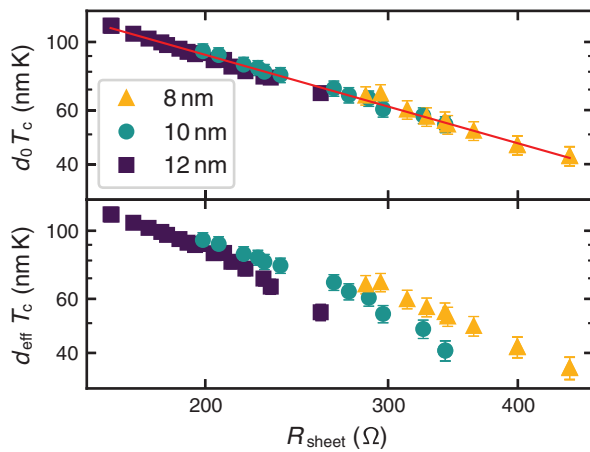
$$d T_c = A R_{\text{sheet}}^{-B}, \quad (\text{D1})$$

which relates film thickness, critical temperature, and sheet resistance. **Figure D1** shows the critical temperature, multiplied with the thickness of





**Figure C1.** SDE of differently irradiated SNSPDs versus  $T_c$  of corresponding CLs of three different thicknesses. The relative uncertainty of the SDE is 2%, the uncertainty of the temperature amounts to 50 mK (error bars not shown for clarity). Furthermore, the SDE measurements were performed at a wavelength of 780 nm.



**Figure D1.** Critical temperature multiplied with film thickness versus sheet resistance, including statistical errors. In the upper plot the thickness of the non-irradiated film is used, while the effective thickness used in the lower plot accounts for surface sputtering and intermixing at the film/substrate interface due to He ion irradiation. The red line in the upper plot is a fit according to the universal scaling law introduced by Ivry et al.,<sup>[69]</sup>  $d_0 T_c = AR_{\text{sheet}}^{-B}$ .

the non-irradiated film,  $d_0 T_c$ . Evidently, this quantity exhibits a linear dependence on the sheet resistance on a log–log scale. As the data of the differently irradiated 8, 10, and 12 nm thick films approximately collapse on a single line, we choose one joint fitting function to determine the constants  $A$  and  $B$  of the universal scaling law and obtain the unitless constants  $A = 1.44 \times 10^4$  and  $B = 0.957$ , provided that the data for  $d$ ,  $T_c$ , and  $R_{\text{sheet}}$  are given in nm, K, and  $\Omega$ , respectively. With these parameters, we obtain the fitting functions shown in Figure 8.

It is interesting to note that the linearity of the three data sets shown in the upper part of Figure D1 is lost when multiplying  $T_c$  with the effective thickness  $d_{\text{eff}} = d_0 - r_s F$  instead of the thickness before irradiation, as shown in the lower part of Figure D1. As introduced in Section 3.2, this reduction of the effective thickness by 0.94 nm per 1000 ions  $\text{nm}^{-2}$  accounts for surface sputtering and intermixing at the film/substrate in-

terface. At present, we can only give a qualitative explanation why the effective thickness is important to describe the continuous increase of  $R_{\text{sheet}}$  in Figure 7 and why it is not relevant for describing  $T_c$ : Via AFM measurements, we observed a surface roughening by He ion irradiation due to surface sputtering and redeposition. Considering now a thin slab of the rough surface, parallel to the sample plane, it consists of many connected islands of NbTiN (or an oxide thereof). On the one hand, this slab has a higher resistivity in the normal conducting state due to the voids; on the other hand, it should have a  $T_c$  similar to a slab without voids as long as the voids are smaller than the coherence length of the superconductor. Of course, further investigation is necessary to better understand the role of surface sputtering and intermixing at the film/substrate interface as well as their influence on thickness, sheet resistance, and critical temperature of the thin film.

Another approach to evaluate our data with the universal scaling law is based on the observation by Ivry et al.<sup>[69]</sup> that the parameters  $A$  and  $B$  are correlated and tend to be higher for amorphous films. Since He ion irradiation induces defects in the superconducting film, one might expect an increase in the parameters  $A$  and  $B$  with increasing He ion fluence. To investigate this in more detail, we fit the universal scaling law to the data in the lower part of Figure D1, where an effective film thickness reduction was taken into account. However, this time we use an individual universal scaling law fit function for each set of data points that share the same He ion fluence (although this means that we only have 2–3 data points for each fit) and account for the thickness reduction with increasing He ion fluence,

$$d_{\text{eff}} T_c = AR_{\text{sheet}}^{-B} \quad (\text{D2})$$

The resulting parameters  $A$  and  $B$  are shown in Figure D2a. It is worth noting that we now have two fit parameters per He ion fluence, making a total of 24 parameters. We observe a correlation between  $A$  and  $B$  similar to that in Figure 5a of the publication by Ivry et al.<sup>[69]</sup> Therefore, we can reduce the number of fit parameters by performing a linear fit of the logarithmically plotted data and obtain the expression

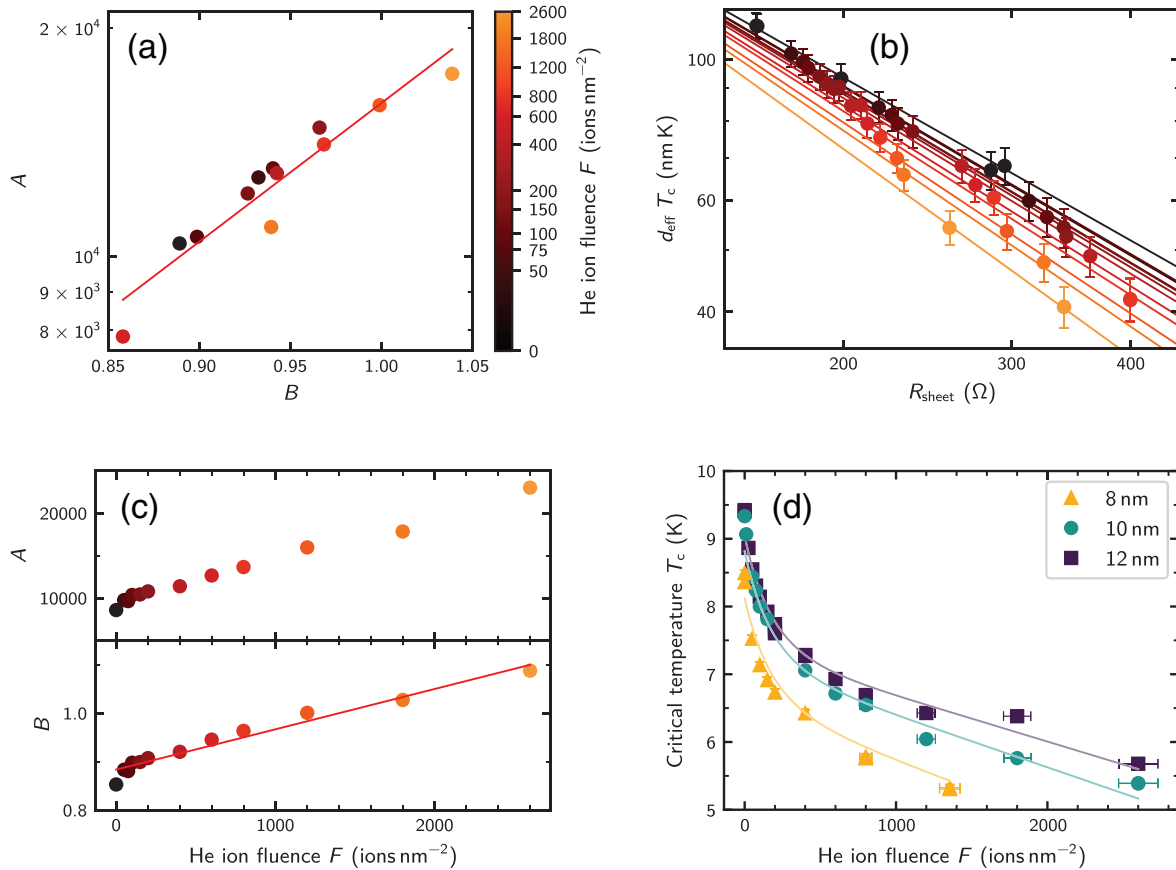
$$A(B) = \exp(4.20B + 5.47924), \quad (\text{D3})$$

shown as red line in Figure D2a. Next, we re-evaluate our data in the lower part of Figure D1 by fitting the universal scaling law to the same data as before, but using Equation (D3) to express  $A$  by  $B$ , thereby reducing the number of fit parameters per He ion fluence to one (hence 12 instead of 24 fit parameters in total). The resulting fit functions and the parameters  $A$  and  $B$  for each He ion fluence are shown in Figure D2b and D2c, respectively. The continuous increase of  $A$  and  $B$  with increasing He ion fluence agrees with the observation of Ivry et al.<sup>[69]</sup> that the more amorphous films have higher values for  $A$  and  $B$ . To obtain a continuous function for  $T_c$  similar to that in Figure 8, we use a linear fit as shown in Figure D2c (red line) to describe the He ion fluence dependence of the parameter  $B$  by

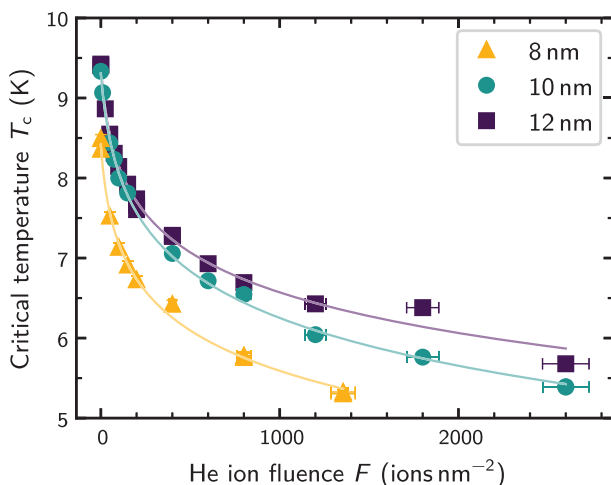
$$B(F) = 8.31 \times 10^{-5} F + 0.88368. \quad (\text{D4})$$

Finally, using Equations (D2)–(D4), we calculate  $T_c(F)$  as shown in Figure D2d. The advantages of this method compared to the simpler fitting procedure at the beginning of this section are, first, that we have taken into account the effective thickness reduction due to He ion irradiation and, second, that the increasing values for  $A$  and  $B$  with increasing He ion fluence support the model of defect cluster formation due to He ion irradiation. On the other hand, this method involves more fitting steps and more fitting parameters than the simpler procedure that yields all three fits in Figure 8 with only two parameters.

In a recent publication, Ruhtinas and Maasilta<sup>[73]</sup> suggest an empirical logarithmic fit function as another alternative for the dependence of the critical temperature on the He ion fluence. As shown in Figure D3, this fit function describes our data for the 12nm thick film even a bit better than the universal scaling law in Figure 8. However, the logarithmic fit requires three fit parameters for each thickness (nine parameters in total), whereas



**Figure D2.** Procedure for fitting the universal scaling law, Equation (D2), to the data shown in the lower part of Figure D1, where the effective thickness reduction due to surface sputtering during He ion bombardment is taken into account. a) The resulting parameters  $A$  and  $B$  after performing a universal scaling law fit for each set of data points of devices irradiated with the same He ion fluence (color coded), given by the data in the lower part of Figure D1. The red line is a linear fit of these correlated parameters in the log-linear plot. b) Re-evaluation of the universal scaling law fits for each set of data points of the same He ion fluence after substituting  $A$  in Equation (D2) by Equation (D3). The resulting parameters  $A$  and  $B$  are shown in (c) along with a linear fit (red) to obtain an expression for the He ion fluence dependence of  $B$ . Finally, the expressions for  $A(B)$  and  $B(F)$ , Equations (D3) and (D4), can be used with Equation (D2) to obtain the continuous functions  $T_c(F)$  shown in (d).



**Figure D3.** Critical temperature versus He ion fluence as shown in Figure 8, including statistical errors. In contrast to the fit with the universal scaling law in Figure 8, we fit our data here with a logarithmic function,  $T_c(F) = -a \log(F + b) + c$ , and fit parameters  $a$ ,  $b$ , and  $c$  for each of the three thicknesses as suggested by Ruhtinas and Maasilta.<sup>[73]</sup>

the universal scaling law fit in Figure 8 requires only two fit parameters to describe all three data sets.

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## Conflict of Interest

The authors declare no conflict of interest.

## Data Availability Statement

The data that support the findings of this study are openly available in Harvard Dataverse at <https://doi.org/10.7910/DVN/5XPXG8>.

## Keywords

He ion irradiation, radiation damage, superconducting nanowire single-photon detector array, superconducting thin film, transport measurement

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