



Effect of Large Disturbances on the Local Behavior of Nonlinear Physically Interconnected Systems



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Motivation – Sensitivity in electric power systems: Subcritical instability & Ill-conditionedness

- [2]: In *highly loaded situations*, inherent tolerance to local small variations reduces and the power systems moves from being elastic to *brittle*.

- [3]: Increasing load leads to *increasing condition number* of power flow Jacobian. *Voltage instability* is related to singularity.

$$\Delta y = J_{PF}^{-1} \Delta x \quad y = (\Theta \quad V)' \quad \text{Voltage angle / magnitude}$$

$$x = (P \quad Q)' \quad \text{Active / reactive powers}$$

$$\kappa(J_{PF}) = \|J_{PF}\| \cdot \|J_{PF}^{-1}\| = \frac{\sigma_{\max}(J_{PF})}{\sigma_{\min}(J_{PF})}, \quad \sigma_{\min} \searrow 0, \quad \kappa \nearrow \infty$$

$$\kappa \approx 10^3$$

- [4]: *Interacting complex modes* may cause *subcritical* oscillatory instability.

→Q1: *What is the role of ill-conditioning rather than singularity?*

→Q2: *How are static behavior and dynamic behavior interrelated?*

Approach: Gateaux differentials & Constrained optimization

- The first variation of a nonlinear function has an expression as *inner product* via the formalism of *Gateaux* differentials, i.e.

$$\delta\lambda = \lim_{\tau \rightarrow 0^+} \frac{\lambda^+(z_{\text{opt}} + \tau \delta z_{\text{opt}}(d)) - \lambda(z_{\text{opt}})}{\tau} = \tau \langle \mathcal{S}_d, d \rangle$$

→ *Eigenvalue moves along gradient* (most sensitive dir.)

- *Gradient* determined via *constrained (Lagrangian) optimization*
→ Define the *Lagrangian*: (max spectral deviation s.t. EVP)

$$\mathcal{L}(\lambda^+, v, \mu, z_{\text{opt}}^+(d)) = \|\delta\lambda\| - \langle \mu, [\lambda^+ B - A(z_{\text{opt}}^+(d))] v \rangle$$

→ *Stationarity & Gateaux differential*

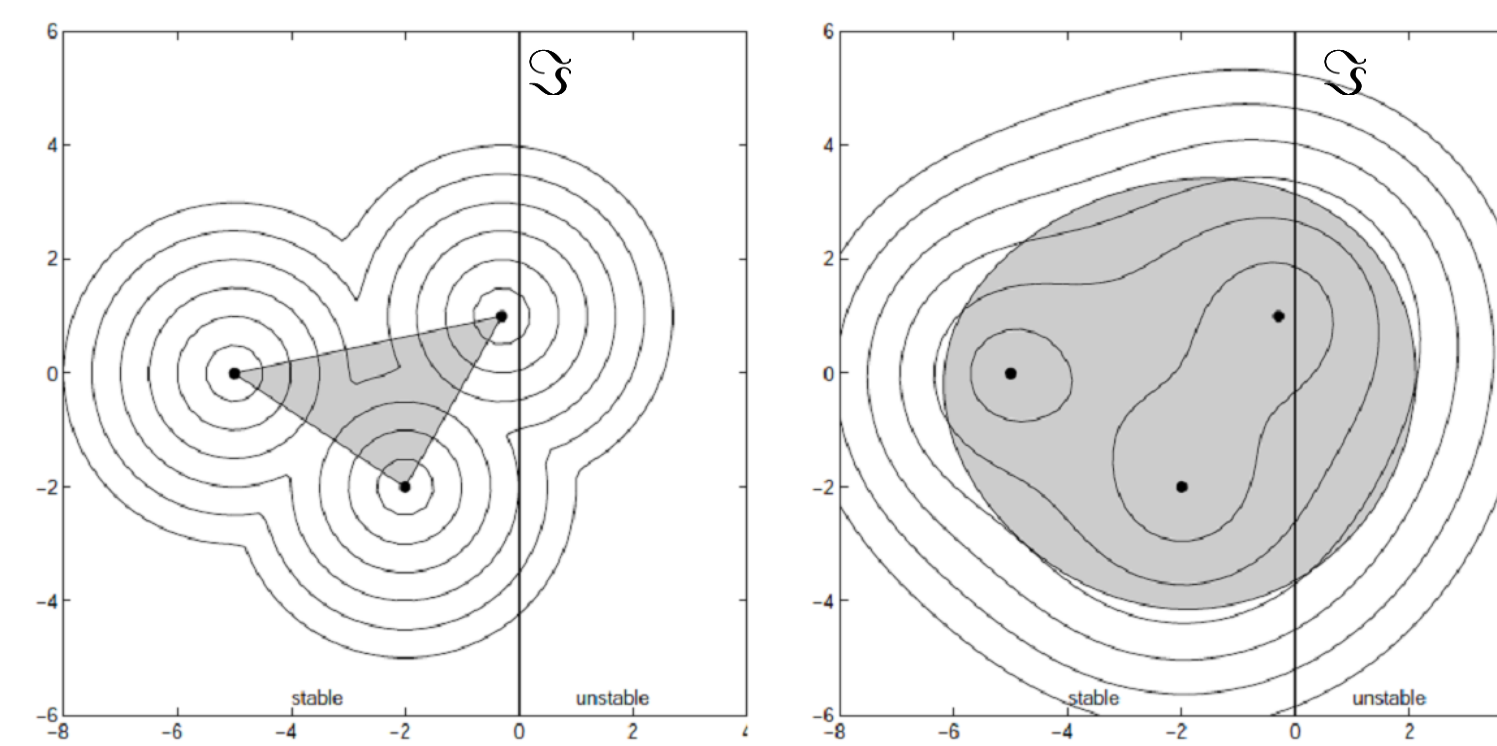
$$\delta\mathcal{L} \stackrel{!}{=} 0 \Rightarrow \mathcal{S}_d$$

= *Necessary optimality conditions & Conditional equations for the gradient*

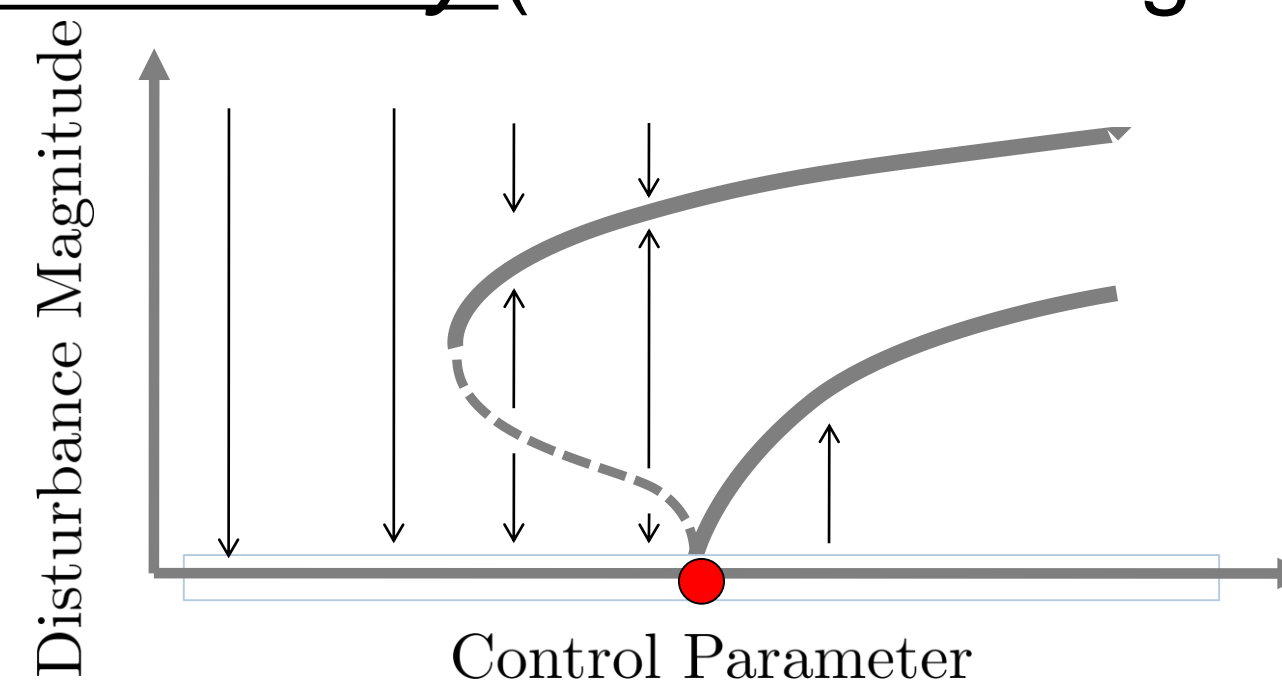
Effect of transport mechanisms in distributed physical systems

[1]:

→ *Ill-conditioned* linearized dynamics
→ Eigenvalue *sensitivity*



→ *Subcriticality* (from interacting modes)



Differences to classical eigenvalue sensitivity

→ Independent of chosen coordinate system! [5]

→ Disturbance input vector contains structural information

(Matrix valued perturbation of local dynamics results from (nodal) disturbance input vector)

Problem Setting: Physically Interconnected systems

System class:

→ System of *nonlinear DAEs*

$$\dot{x} = f(x, y)$$

$$0 = g(x, y)$$

$$J_{PF} = \nabla_y g|_{z_{\text{opt}}}$$

→ has *steady state* operating point (with state $z = (x, y)'$)

$$z_{\text{opt}} \leftarrow \mathcal{R}(z) := \begin{bmatrix} f(x, y) \\ g(x, y) \end{bmatrix} = 0$$

→ serving as set-point for *controlled local dynamics*

$$\frac{d}{dt} \begin{pmatrix} \Delta x \\ 0 \end{pmatrix} = \underbrace{\begin{bmatrix} \nabla_x f|_{z_{\text{opt}}} & \nabla_y f|_{z_{\text{opt}}} \\ \nabla_x g|_{z_{\text{opt}}} & \nabla_y g|_{z_{\text{opt}}} \end{bmatrix}}_{\nabla_z \mathcal{R}(z)|_{z_{\text{opt}}} = A(z_{\text{opt}})} \begin{pmatrix} \Delta x \\ \Delta y \end{pmatrix}$$

→ *Local dynamics determined by spectral properties*:

$$A(z_{\text{opt}})v = \lambda Bv$$

Consider a steady forcing, so that $\mathcal{R}(z_{\text{opt}}^+) = d$, then,

$$d \xrightarrow{\mathcal{R}+d=0} \delta z = z_{\text{opt}}^+ - z_{\text{opt}} \xrightarrow{Av=\lambda Bv} \delta\lambda = \lambda^+ - \lambda$$

→Q3: *How to quantify the change in eigenvalue?*

Main result & Implications: Power flow Jacobian & Subcriticality

→A3: *Theorem*: Estimate for deviations

$$\delta\lambda = \tau \left\langle \left(\left[\nabla \mathcal{R}(z)|_{z_{\text{opt}}} \right]^{-1} \right)^* \mathcal{S}_z, d \right\rangle$$

Spectral sensitivity $\mathcal{S}_z = \left[\nabla_z [A(z_{\text{opt}})v]|_{z_{\text{opt}}} \right]^* w$

Adjoint eigenvector $w = \mu$

→ A2: *Inverse of steady state Jacobian acts as gain matrix on eigenvalue sensitivity!*

→ A1: *Condition number ~ worst case amplification*

In simple models $J_{PF} = \nabla_z \mathcal{R}$

$$\|J_{PF}^{-1}\| = \frac{1}{\sigma_{\min}(J_{PF})} \xrightarrow{\text{loading} \uparrow} \infty$$

Else, relations between J_{PF} & $\nabla_z \mathcal{R}$ can be characterized using function maps (and their gradients) as introduced in [6]

Discussion & Outlook

→ *Power flow not considered in linear models* (for RT control) but interaction of the two has caused recent large blackouts!

→ Large amplification possible scenario for *subcritical Hopf-bifurcation*

→ New, *combined static/dynamic analysis tools*, as in [7]

[1]: L.N. Trefethen and M. Embree, "Spectra and Pseudospectra – The behavior of Nonnormal Matrices", Princeton University Press, 2008

[2]: International Energy Agency, "Empowering variable renewables – Options for flexible electricity systems", Technical Report, 2008.

[3]: Y. Wang, L.C. Da Silva, W. Xu, and Y. Zhang, "Analysis of ill-conditioned power-flow problems using voltage stability methodology", Generation, Transmission and Distribution, 2001

[4]: Ian Dobson, J. Zhang, S. Greene, H. Engdahl, and Peter W. Sauer, "Is strong modal resonance a precursor to power system oscillations?", IEEE Transactions on Circuits and Systems I, 2001

[5]: P. Meliga, D. Sipp, and J.M. Chomaz, "Open-Loop Control of Compressible Afterbody Flows Using Adjoint Methods", Physics of Fluids, 2010

[6]: G.Y. Cao and D. Hill, "Power Systems Voltage Small-Disturbance Stability Studies Based on the Power Flow Equations", IET Generations, Transmission, Distribution, 2010

[7]: H. Mangesius, M. Huber, T. Hamacher, S. Hirche, "A Framework to Quantify Technical Flexibility in Power Systems Based on Reliability Certificates", IEEE ISGT, 2013